

**Exterior Brick Masonry Veneer
Supported by Metal Plate Connected
Wood Trusses (MPCWT)**

Design Guide

Revised 11/17/2016

SBCA

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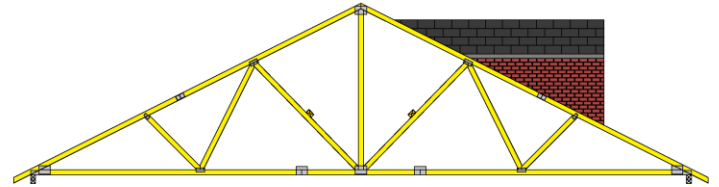
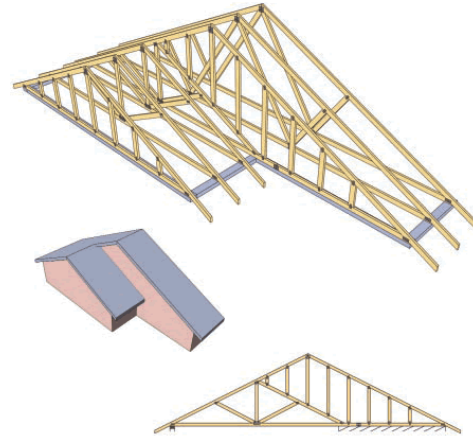
Introduction

- The *IRC 2015* includes no prescriptive provisions to specifically address an exterior brick veneer wall supported directly by MPCWT
- Code compliance can be accomplished by both individual designs and by adhering to the guidance in this presentation



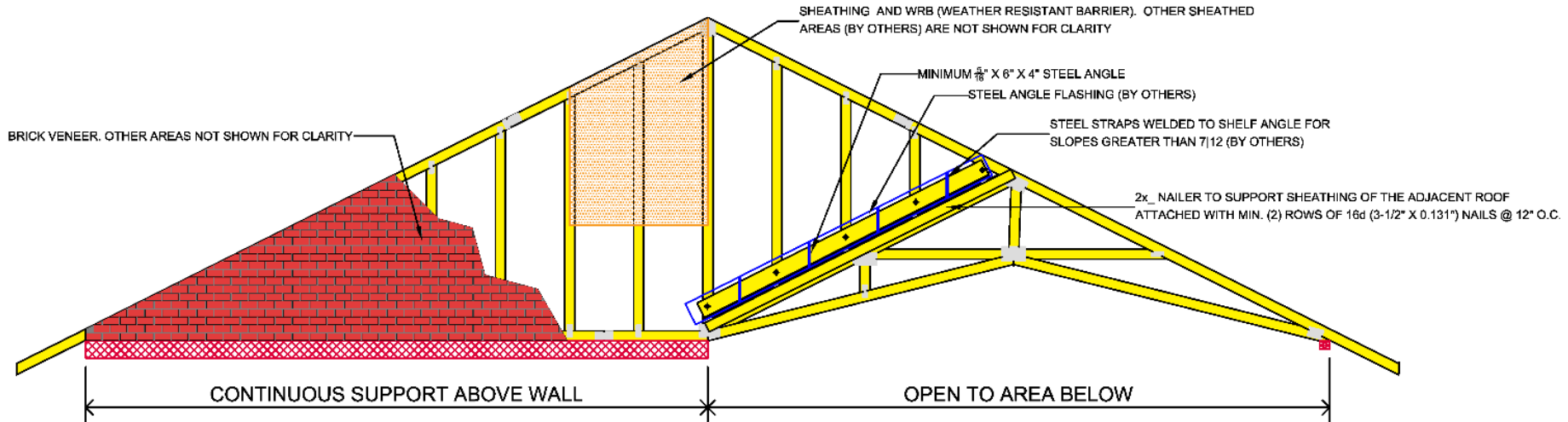
Introduction

- This presentation specifically focuses on the gable end at the transition from a wider section of a building to a narrower section
- However, the concepts shown can be applied to many different situations utilizing trusses, such as supporting brick veneer at dormer locations.



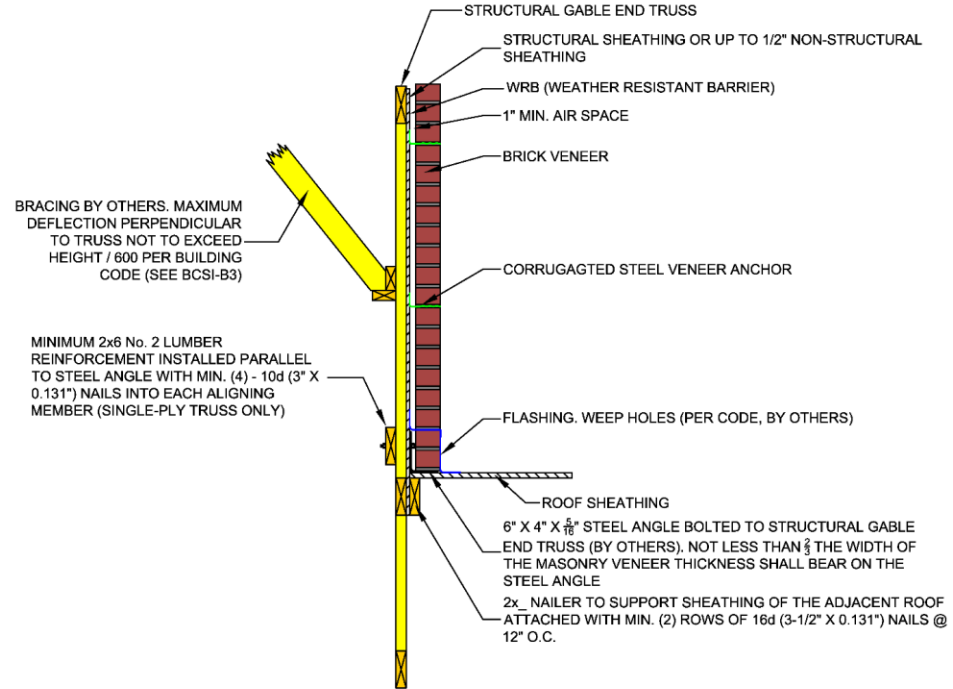
Step 1: Review Detail

- The detail below may be referred to by the building designer to achieve a code-conforming steel lintel connection



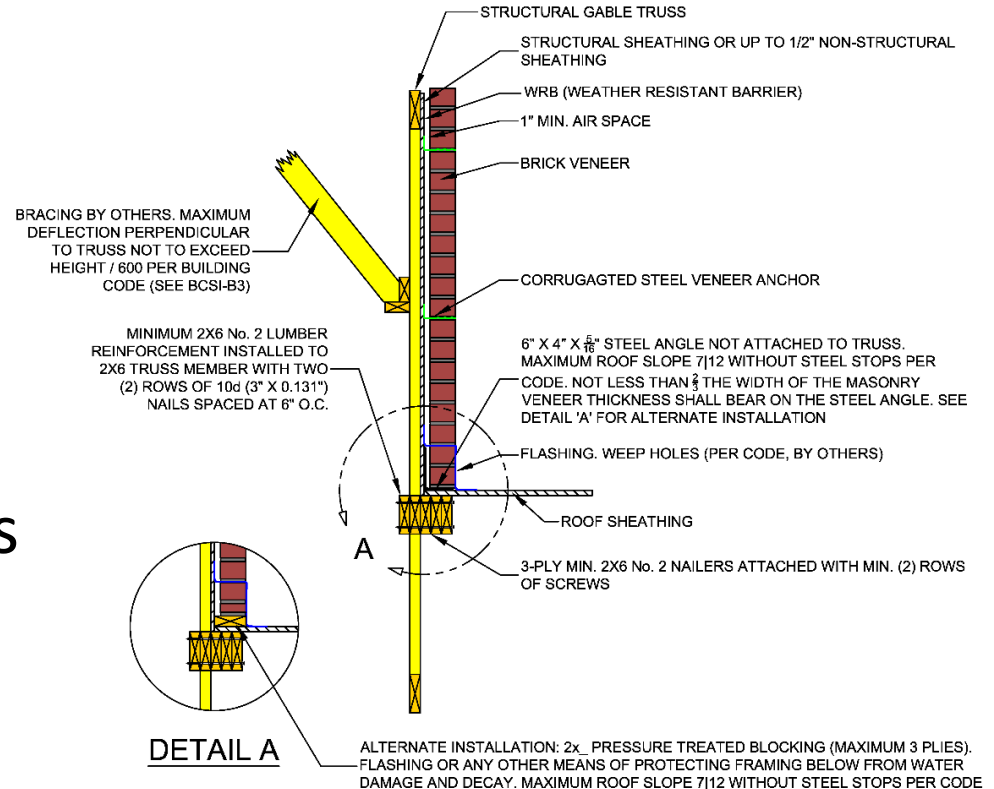
Step 1: Review Detail

- Section view of previous slide
- Note that sheathing must be covered with a water-resistant membrane, unless the sheathing is water resistant and the joints are sealed.



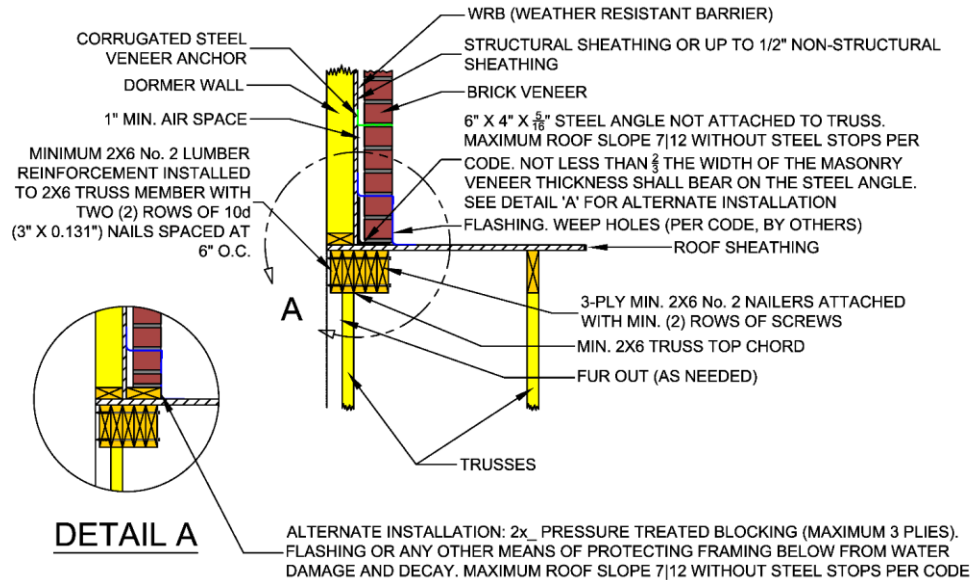
Step 1: Review Detail

- An alternative connection using (3) 2x6's to support the brick masonry veneer directly above the 2x6's



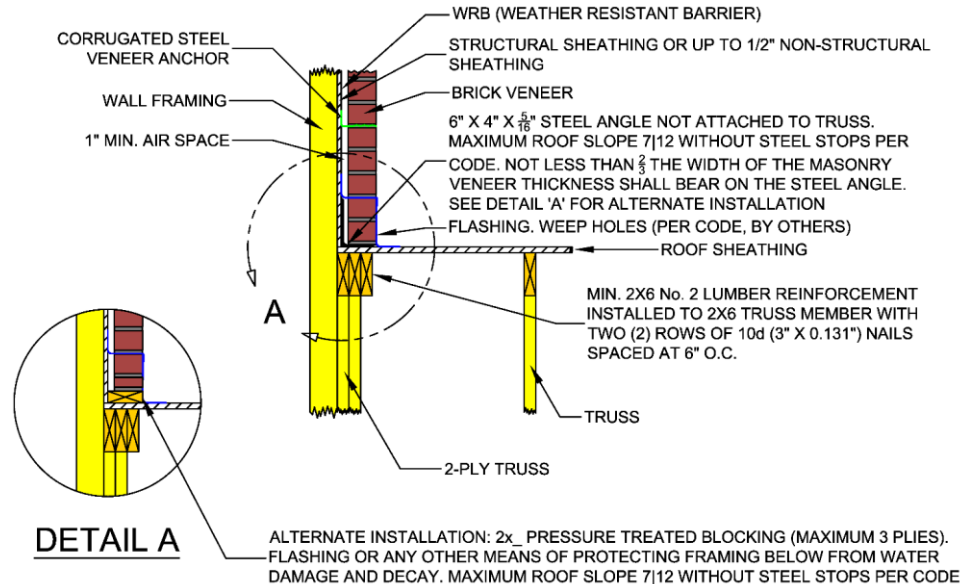
Step 1: Review Detail

- Another alternative connection using (3) 2x6's to support the brick masonry veneer:



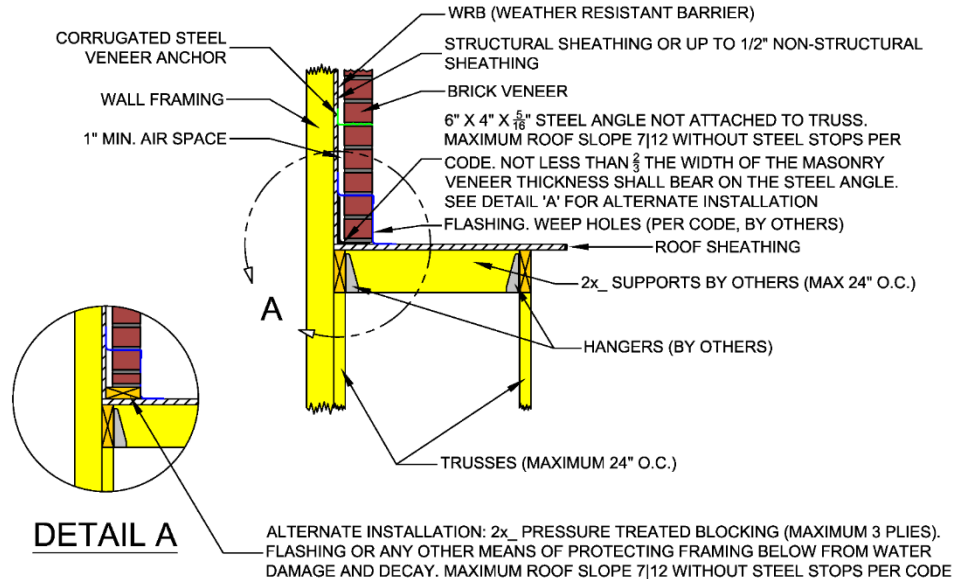
Step 1: Review Detail

- An alternative connection using 2-ply MPCWT directly below to support the brick masonry veneer:



Step 1: Review Detail

- An alternative connection using 2x_ material between MPCWT to support the brick masonry veneer:



Step 2: Verify Design Values

- Truss total load deflection is limited to $L/600$
- Load Duration factor is $C_D=0.9$
- Creep factor for long-term deflection calculation shall be 1.5 for dry lumber and 2.0 for unseasoned lumber
 - Creep is defined as time-dependent deformation of a structural member under constant load. In this case brick dead load is a constant and/or sustained load (see ANSI/TPI 1-2002, 2007)
- Maximum weight of brick masonry veneer is 40 psf
- Maximum height of brick masonry is 12'-8" per the IRC

Step 3: Select Lintel

- A minimum 6" x 4" x 5/16" (152 mm by 102 mm by 8 mm) steel angle, with the long leg placed vertically, shall be anchored to MPCWT using bolts per the following tables
- For assemblies with Structural Sheathing:

Bolt Spacing (Truss Vertical Member Spacing)	Bolt Diameter ^{1,b} With Structural Sheathing (OSB, Plywood)			
	3/8-inch bolt diam.	1/2-inch bolt diam.	5/8-inch bolt diam.	3/4-inch bolt diam. ²
24 inches o.c. ^c	Max. 4'-6" brick height	Max. 6'-1" brick height	Max. 7'-9" brick height	Max. 9'-5" brick height
16 inches o.c. ^c	Max. 6'-11" brick height	Max. 9'-5" brick height	Max. 11'-10" brick height	Max. 14'-3" ^a brick height
12 inches o.c. ^c	Max. 9'-4" brick height	Max. 12'-8" brick height	Max. 15'-11" ^a brick height	Max. 19'-2" ^a brick height

¹ Bolt shear capacity is calculated based on 2015 NDS for Wood Construction for lumber with Specific Gravity G=0.42 (Spruce-Pine-Fir) with moisture content less than 19% and the following adjustment factors: C_D=0.9, C_t and C_M=1.0.

² Use only with minimum 2x4 vertical truss members. F_{em}=4700 psi, F_{es}=87000 psi, 5/16" Steel, no gap, Bolt F_{yb}=45000 psi
Brick weight up to 40 PSF.

^a The maximum height of brick masonry veneer above the steel angle support using prescriptive requirements of 2015 IRC shall be 12'-8". Weight of brick shall be included in truss design.

^b Pre-drill oval holes in the shelf angle for easier field installation adjustment.

^c It must be noted that the design of the truss only accounts for the gravitational loads in the plane of the truss. The building designer needs to adequately account for loads normal to the face of the truss and the bracing/restraint of the roof and wall system.

Step 3: Select Lintel

- For assemblies with Non-Structural Sheathing:

Bolt Spacing (Truss Vertical Member Spacing)	Bolt Diameter ^{1,b} With up to ½" of Non-Structural Sheathing (Weather Resistant Barrier, Insulation, etc.)			
	3/8-inch bolt diam.	1/2-inch bolt diam.	5/8-inch bolt diam.	3/4-inch bolt diam. ²
24 inches o.c. ^c	Max. 3'-1" brick height	Max. 4'-4" brick height	Max. 5'-6" brick height	Max. 6'-8" brick height
16 inches o.c. ^c	Max. 4'-9" brick height	Max. 6'-8" brick height	Max. 8'-5" brick height	Max. 10'-3" brick height
12 inches o.c. ^c	Max. 6'-6" brick height	Max. 9'-0" brick height	Max. 11'-5" brick height	Max. 13'-9" ^a brick height

¹ Bolt shear capacity is calculated based on 2015 NDS for Wood Construction for lumber with Specific Gravity G=0.42 (Spruce-Pine-Fir) with moisture content less than 19% and the following adjustment factors: $C_D=0.9$, C_t and $C_M=1.0$.

² Use only with minimum 2x4 vertical truss members. $F_{em}=4700$ psi, $F_{es}=87000$ psi, 5/16" Steel with ½" gap between steel and truss, Bolt $F_{yb}=45000$ psi, Brick weight up to 40 PSF.

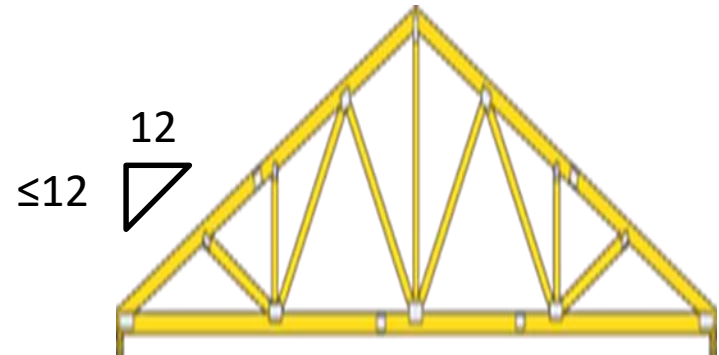
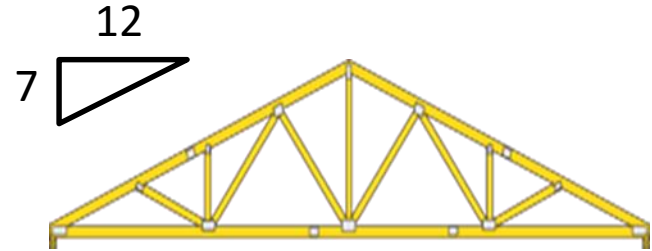
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^b Pre-drill oval holes in the shelf angle for easier field installation adjustment.

^c It must be noted that the design of the truss only accounts for the gravitational loads in the plane of the truss. The building designer needs to adequately account for loads normal to the face of the truss and the bracing/restraint of the roof and wall system.

Step 4: Determine if Stops are Needed

- The maximum slope of the roof construction without stops welded to the steel angle shall be 7:12
- Trusses supporting veneer with slopes between 7:12 and 12:12 shall have stops of a minimum 3" x 3" x 1/4" (76 mm x 76 mm x 6 mm) steel plates welded to the angle at max. 24" (610 mm) o.c. along the angle or as approved by the building official



Step 5: Select Ties

- Stainless steel ties specified under ASTM [A 240](#) or [A 580](#)
- Corrosion protected ties such as zinc coated corrugated steel ties, minimum 22 U.S. gauge thick (0.0299"), 7/8" x 6" (0.76mm x 22 mm x 152 mm) complying with ASTM [A 653](#) and [A 153](#) class B2



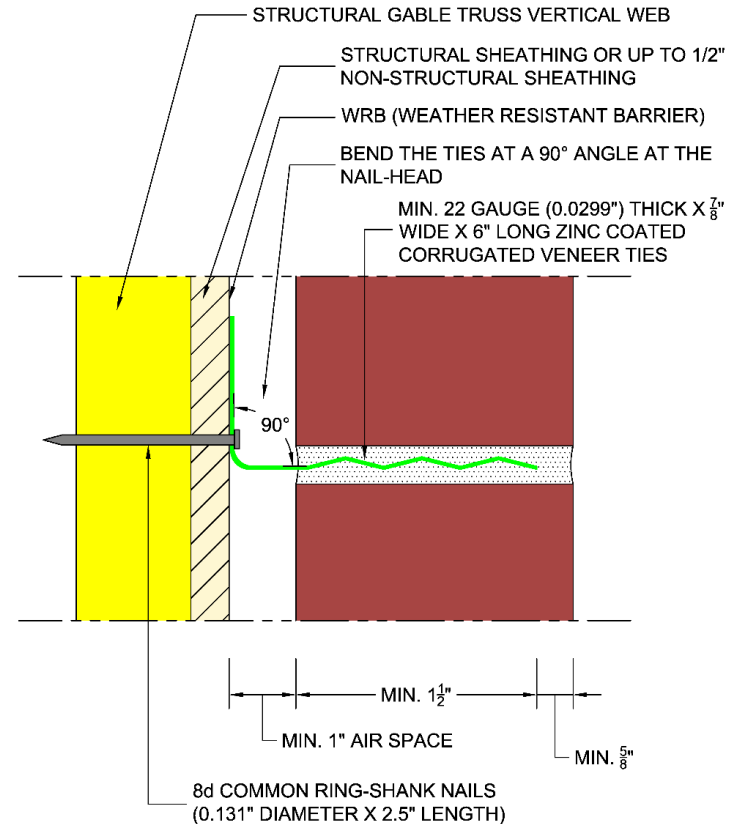
Step 5: Select Ties

- Strand wire ties are less susceptible to corrosion than corrugated steel sheet ties
- Minimum strand wire size diameter shall be 9 U.S. gauge [(0.148") or (4 mm)] and be spaced same as corrugated steel ties and shall have a hook embedded in the mortar joint



Step 6: Select Tie Spacing

- Veneer ties shall be spaced at maximum 32" o.c. (610 mm) horizontally and 24" o.c. vertically and shall support max 2.67 ft² (0.25 m²) of brick veneer wall area
- For new construction, wall stud spacing of 16" o.c. is recommended so that ties can be anchored at this spacing



Step 6: Select Tie Spacing

- The following tables provides recommendations for maximum vertical tie spacing for high wind areas when structural gable truss vertical members are spaced at 24", 16" and 12" on center spacing
- In the areas that are susceptible to both high wind and seismic loads, masonry brick veneer system should be evaluated by an RDP to ensure that brick veneer cladding can resist both seismic and wind design loads

Step 6: Select Tie Spacing

- Maximum vertical tie spacing for assemblies with structural sheathing

Wind Speed (3-sec Peak Gust)	Wind ^{1,2,9} Pressure (psf)	Maximum Vertical spacing for Ties in inches ^{1,2,3,4,8} 8d (0.131" x 2.5") Ring-Shank Nails With 1/2" Structural Sheathing (OSB, or Plywood) and 2" of Nail penetration ⁴					
		Truss members @ 24" o.c.		Truss members @ 16" o.c.		Truss members @ 12" o.c.	
		SPF	SYP	SPF	SYP	SPF	SYP
115 mph	19.1	16 ⁵	16 ⁵	24 ⁵	24 ⁵	24 ⁵	24 ⁵
120 mph	20.8	16 ⁵	16 ⁵	24 ⁵	24 ⁵	24 ⁵	24 ⁵
130 mph	24.4	16	16 ⁵	24 ⁵	24 ⁵	24 ⁵	24 ⁵
140 mph	28.3	14	16 ⁵	21	24 ⁵	24 ⁵	24 ⁵
150 mph	32.5	12	12 ⁶	18	18 ⁶	24 ⁵	24 ⁵
160 mph	37.0	10	12 ⁶	16	18 ⁶	21	24 ⁵
180 mph	46.8	NA ⁷	NA ⁷	12	18 ^{6,7}	17	18 ⁷

¹ The vertical tie spacing is based on wind loads derived from ASCE 7-10 Components and Cladding – Method 1 (simplified – Figure 30.5-1, Zone 5, Effective wind area = 10 sf), located in Exposure category B, h = 30 ft., importance factor (I=1) and no topographic influence ($K_{zt}=1.0$). For other heights, exposure, importance factor and topographic influence, an engineered design is recommended. Table based on a tie in every vertical.

² Net Design Wind Pressures from ASCE 7-10 Figure 30.5-1 have been multiplied by 0.6 for Allowable Stress Design.

³ Nail withdrawal strength is for truss lumber with Specific Gravity G=0.42 (Spruce-Pine-Fir (SPF)) and G=0.55 (Southern Yellow Pine (SYP)) with moisture content less than 19% and the following adjustment factors: $C_D=1.0$, $C_L=0.8$, C_M , C_{eg} , and $C_{in}=1.0$. See [FEMA Technical Fact Sheet No. 5.4 Attachment of Brick Veneer in High-Wind Regions](#).

$W = 1800G^2D \times 1.6$ SPF NV = 66.55 SYP NV = 114.12

⁴ Nail embedment depth of 2" was assumed for 8d common ring-shank nails (0.131"-diameter x 2 1/2" long) (1-1/2" truss plus 1/2" structural sheathing). A minimum of 3 (0.131" x 2") nails required attaching the sheathing to the truss for every tie.

⁵ The maximum vertical spacing allowed by the [Brick Industry Association's Technical Notes 28](#) is 24" & requires an anchor for every 2.67 sq. ft. of wall area.

⁶ Where the wind pressure exceeds 30 psf, reduce wall area supported by each anchor to max. 2 SF per the IRC R703.8.4.1 & the [Brick Industry Association's Technical Note 28](#).

⁷ Where wind pressure exceeds 40 psf do not space anchors more than 18" vertically & horizontally per the [Brick Industry Association's Technical Note 28](#).

⁸ Additional anchors required around openings larger than 16" in either dimension. See the IRC or IBC for these requirements.

⁹ It must be noted that the design of the truss only accounts for the gravitational loads in the plane of the truss. The building designer needs to adequately account for loads normal to the face of the truss and the bracing/restraint of the roof and wall system.

Step 6: Select Tie Spacing

- Maximum vertical tie spacing for assemblies with **non-structural sheathing**

Wind Speed (3-sec Peak Gust)	Wind ^{1,2,9} Pressure (psf)	Maximum Vertical spacing for Ties in inches ^{1,2,3,4,8} 8d (0.131" x 2.5") Ring-Shank Nails With Non-Structural Sheathing (Weather Resistant Barrier, Insulation, etc.) and 1-1/2" of Nail penetration in truss member.					
		Truss members @ 24" o.c.		Truss members @ 16" o.c.		Truss members @ 12" o.c.	
		SPF	SYP	SPF	SYP	SPF	SYP
115 mph	19.1	15	16 ⁵	23	24 ⁵	24 ⁵	24 ⁵
120 mph	20.8	14	16 ⁵	21	24 ⁵	24 ⁵	24 ⁵
130 mph	24.4	12	16 ⁵	18	24 ⁵	24 ⁵	24 ⁵
140 mph	28.3	10	16 ⁵	15	24 ⁵	21	24 ⁵
150 mph	32.5	9	12 ⁶	13	18 ⁶	18	24 ⁵
160 mph	37.0	8	12 ⁶	12	18 ⁶	16	24 ⁵
180 mph	46.8	NA ⁷	NA ⁷	9	16	12	18 ⁷

¹ The vertical tie spacing is based on wind loads derived from ASCE 7-10 Components and Cladding – Method 1 (simplified – Figure 30.5-1, Zone 5, Effective wind area = 10 sf), located in Exposure category B, h = 30 ft., importance factor (I=1) and no topographic influence (K_t=1.0). For other heights, exposure, importance factor and topographic influence, an engineered design is recommended. Table based on a tie in every vertical.

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³ Nail withdrawal strength is for truss lumber with Specific Gravity G=0.42 (Spruce-Pine-Fir (SPF)) and G=0.55 (Southern Yellow Pine (SYP)) with moisture content less than 19% and the following adjustment factors: C_p=1.0, C_t=0.8, C_{Nr}, C_{eg}, and C_{in}=1.0. See [FEMA Technical Fact Sheet No. 5.4 Attachment of Brick Veneer in High-Wind Regions](#).

W = 1800G²D x 1.6 SPF NV = 49.9 SYP NV = 85.6

⁴ Nail embedment depth of 1-1/2" was assumed for 8d common ring-shank nails (0.131"-diameter x 2 1/2"-long).

⁵ The maximum vertical spacing allowed by the [Brick Industry Association's Technical Notes 28](#) is 24" & requires an anchor for every 2.67 sq. ft. of wall area.

⁶ Where the wind pressure exceeds 30 psf, reduce wall area supported by each anchor to max. 2 SF per the IRC R703.8.4.1 & the [Brick Industry Association's Technical Note 28](#).

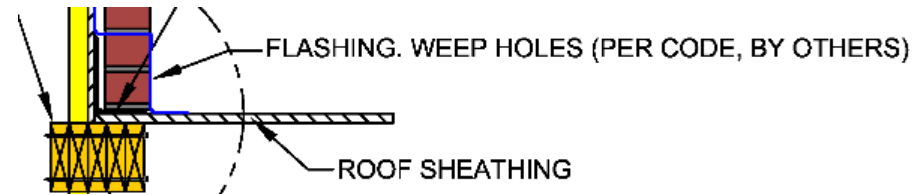
⁷ Where wind pressure exceeds 40 psf do not space anchors more than 18" vertically & horizontally per the [Brick Industry Association's Technical Note 28](#).

⁸ Additional anchors required around openings larger than 16" in either dimension. See the IRC or IBC for these requirements.

⁹ It must be noted that the design of the truss only accounts for the gravitational loads in the plane of the truss. The building designer needs to adequately account for loads normal to the face of the truss and the bracing/restraint of the roof and wall system.

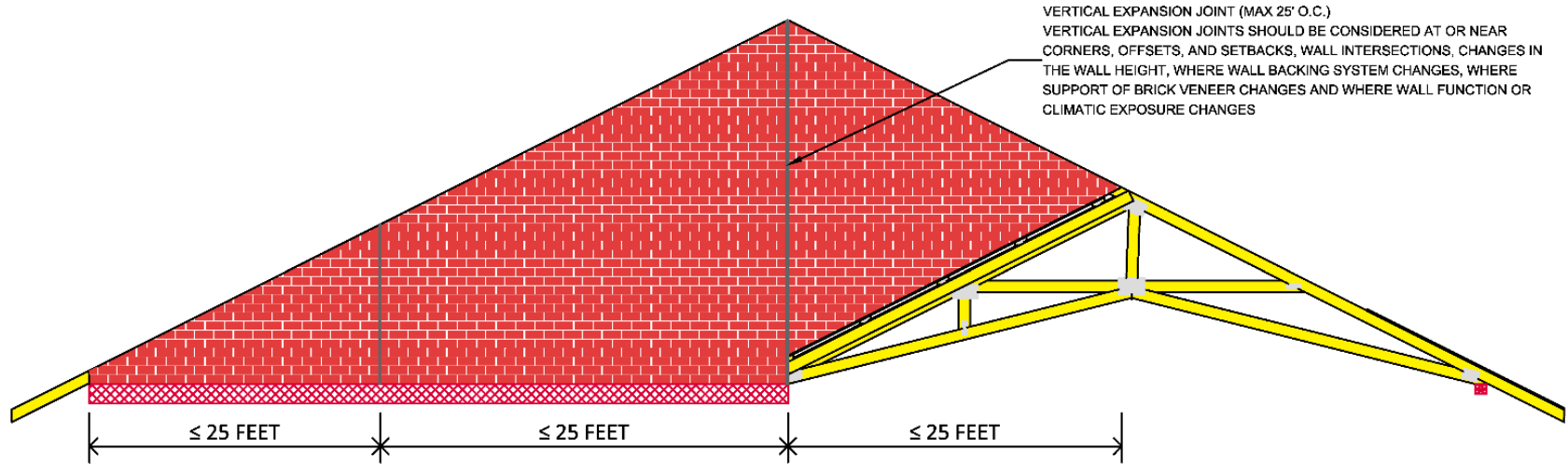
Step 7: Flashing and Weep Holes

- **Flashing and weep holes** shall be located in the brick veneer wythe above the steel angle per the building codes.
- Flashing should consist of normal base flashing, step flashing and counter flashing installed directly on the adjacent (i.e., lower) roof sheathing.
- Weep holes shall be at a maximum spacing of 33" (838 mm) o.c. and shall be not less than 3/16" (5 mm) in diameter.



Step 8: Vertical Expansion Joints

- Create vertical expansion joints @ a maximum 25' (7.6 m) o.c.



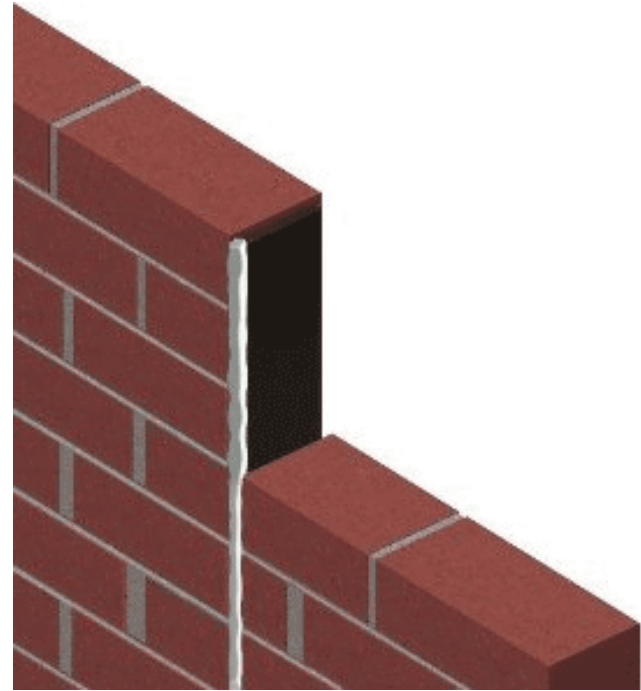
Step 8: Vertical Expansion Joints

- The actual location of vertical expansion joints in a structure depends on the structural configuration as well as the expected amount of horizontal movement
- Expansion joints are typically sized similar to a mortar joint, usually between $\frac{3}{8}$ " (10 mm) and $\frac{1}{2}$ " (13 mm)



Step 8: Vertical Expansion Joints

- Vertical expansion joints should also be considered with:
 - Corners
 - Offsets
 - Setbacks
 - Wall intersections
 - Changes in the wall height
 - Wall backing system changes
 - Brick veneer support changes
 - Wall function or climatic exposure changes



References

- [2015 IRC](#) and [2015 IBC](#)
- Wind loads specified in [ASCE 7-10](#)
- Fastener strengths specified in the [NDS](#)
- Masonry Structures standards contained in [TMS 402/602](#).
- General guidance given in [Brick Industry Association's Technical Notes 18A, 28, 28B](#) and [44B](#)