

PMA Calibration Factors for the MEPDG

Association of Modified Asphalt Producers
12 February 2008

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**APPLIED
RESEARCH
ASSOCIATES, INC.**

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Presentation Overview

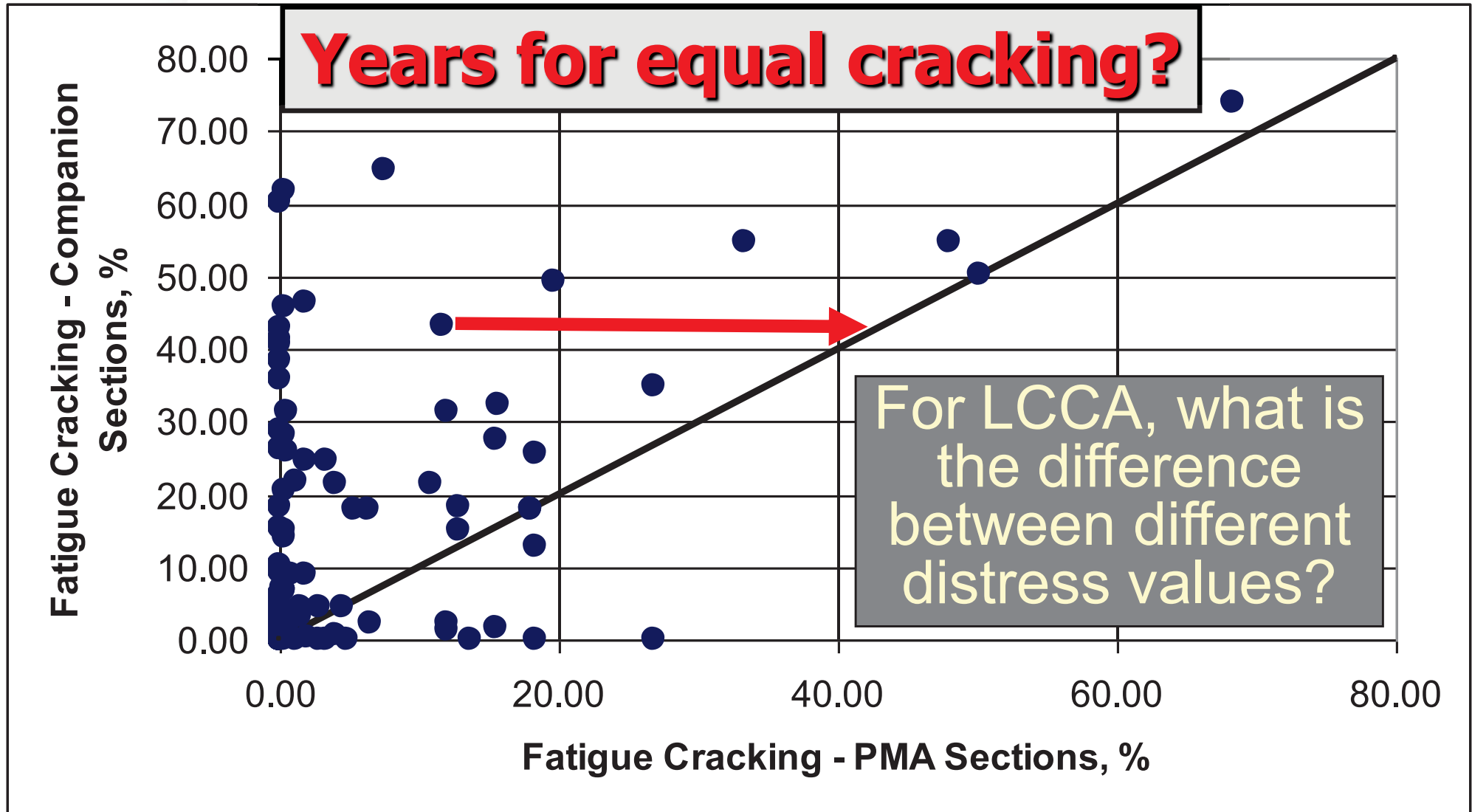
1. Introduction
2. Distress Comparison Update
3. PMA Calibration Factors & the MEPDG
4. Conclusions (Findings & Marketing Issues)

Study Objective

1. Determine the MEPDG calibration factors for PMA mixtures, as compared to neat or unmodified HMA mixtures.

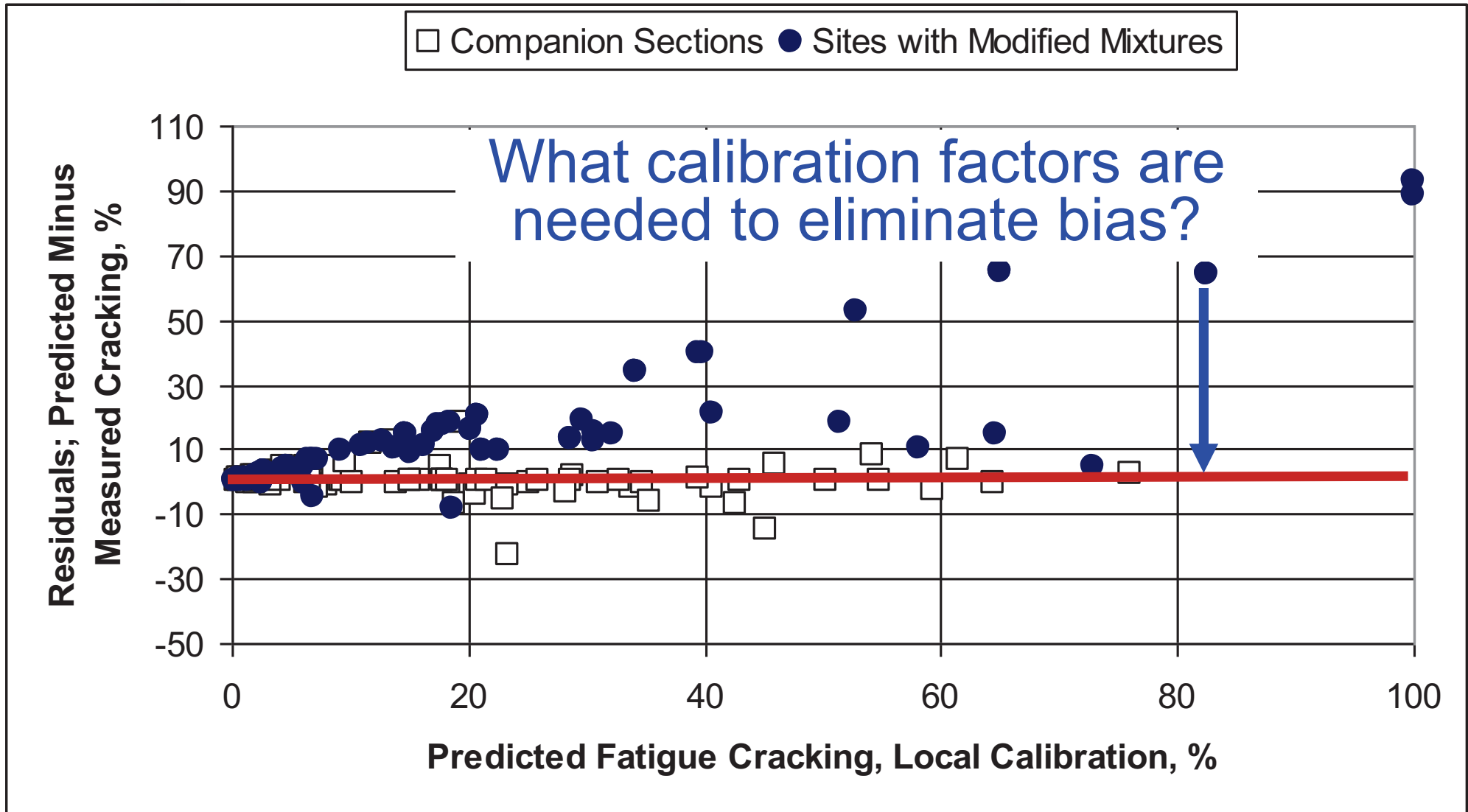
Continuation of: *Quantifying the Effects of PMA for Reducing Pavement Distress*; Report IS-215

Quantifying the Effects of PMA

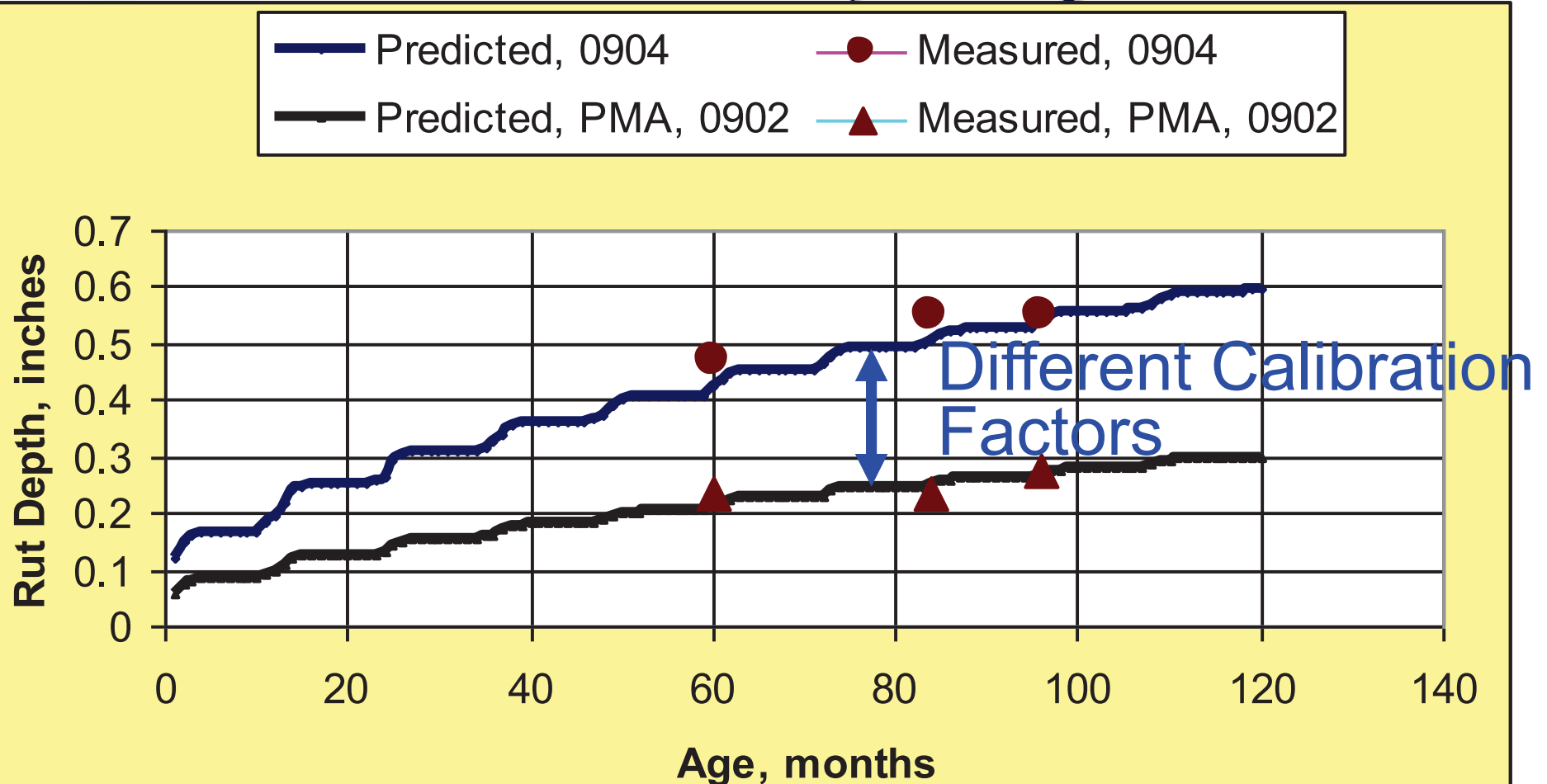


AI Report IS-215

Residuals - Fatigue Cracking



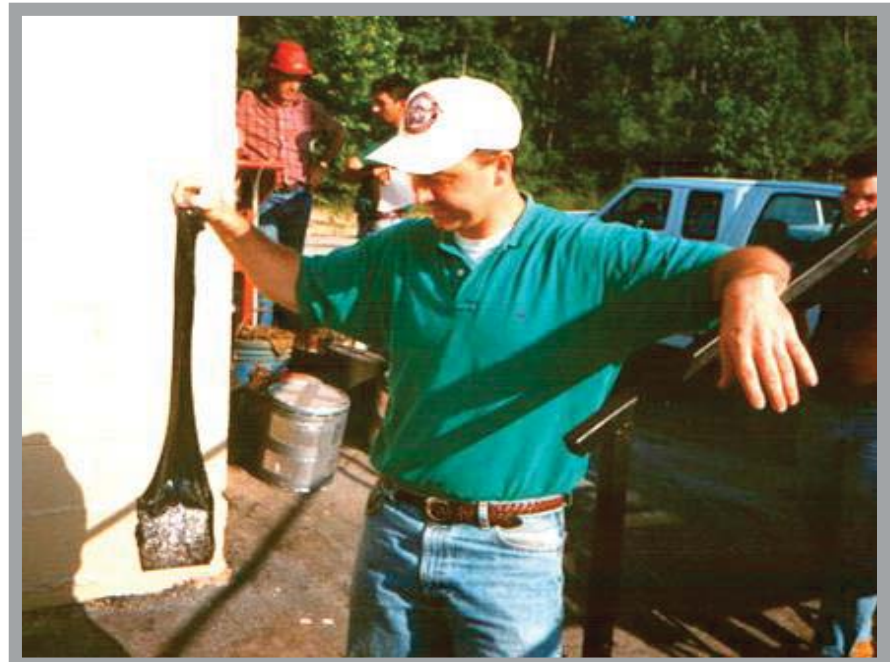
Calibration Study Objective



For Design: What is the calibration factor to eliminate bias between the measured & predicted distress values?

Type of Materials

- Insufficient data to determine material specific effects.
- Most of the test sections included one of the following polymers:
 - Natural latex
 - Synthetic latex
 - Block copolymer
 - Plastics



Cell Specific Calibration

Pavement Cross Section	Foundation	Climate			
		Freeze		Non-Freeze	
		Wet	Dry	Wet	Dry
Thin HMA	Fine-Grained	2	2	4	3
	Medium-Grained	3	3	3	3
	Coarse-Grained	2	2	2	3
Full-Depth	Thin HMA	2	2	3	2
	Coarse-Grained	0	1	2	2
HMA Overlays	HMA	3	3	6	6
	PCC	4	3	4	4
Total No. PMA Sections		16	17	26	25

Neat HMA used for calibration to define time difference

Types of Analyses

1. Comparison of measured distress values using more recent data, **2006**.
2. Determine mix calibration factors & compare neat & PMA values using **Version 1.0 of the MEPDG**.

Slight deviation from initial plan.

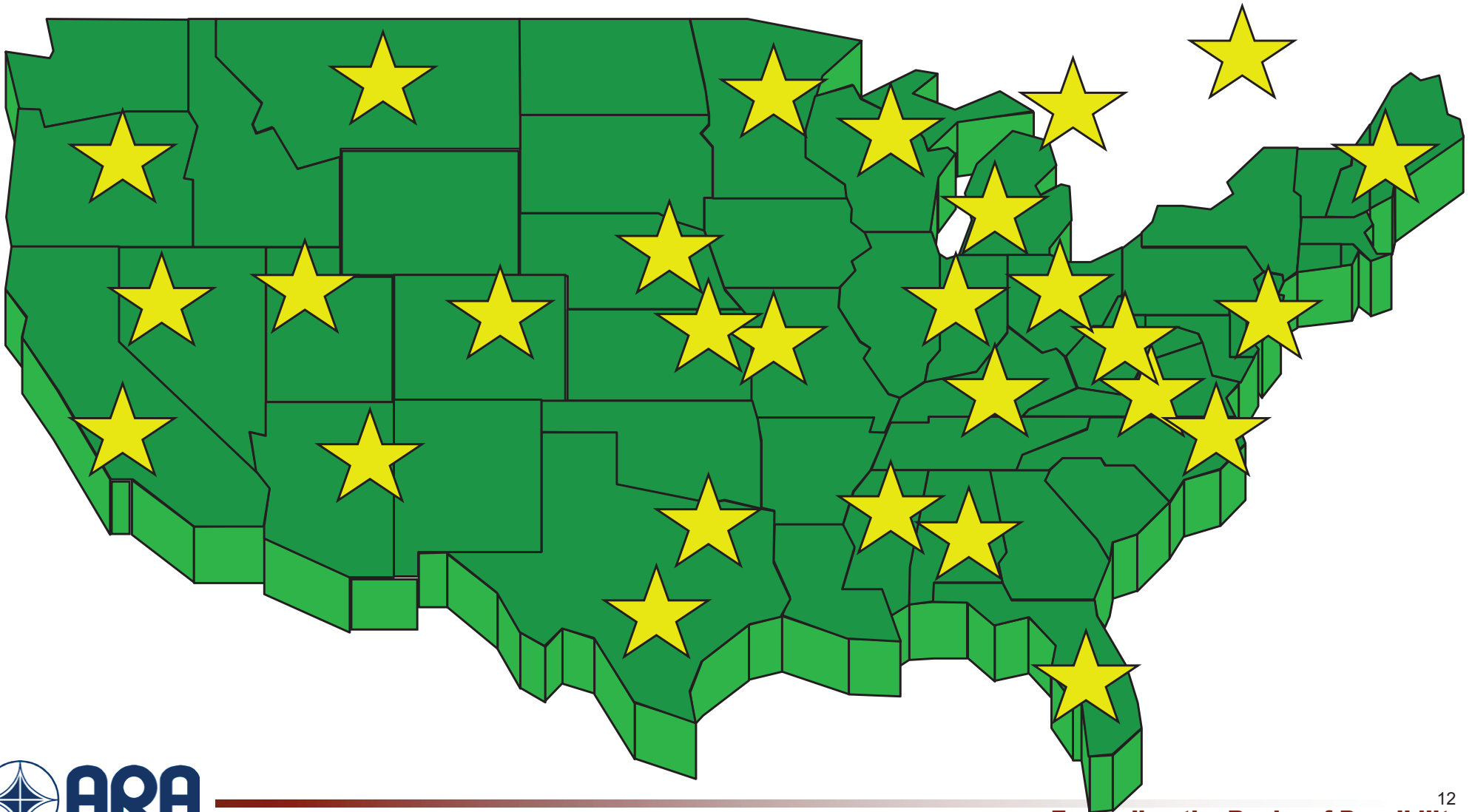
Presentation Overview

1. Introduction
- 2. Distress Comparison Update**
3. PMA Calibration Factors & the MEPDG
4. Conclusions (Findings & Marketing Issues)

Comparison of Pavement Distress/Performance

- ☒ Fatigue Cracking; Area & longitudinal combined
- ☒ Rutting
- ☒ Thermal Cracking

Selected Pavement Locations for Performance Comparisons



Distress Comparison—Rutting

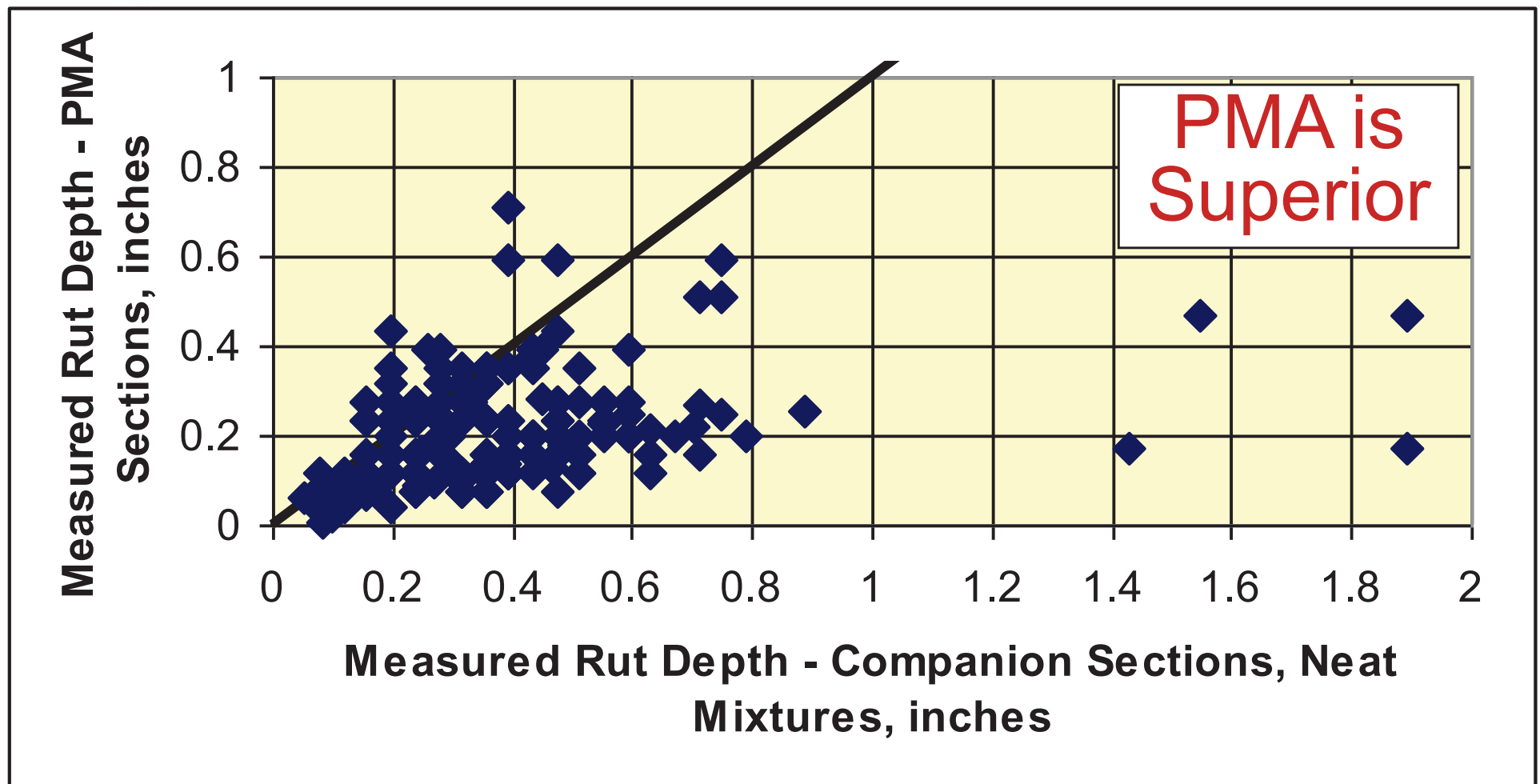


Figure 2 in the report.

Distress Comparison—Fatigue Cracking

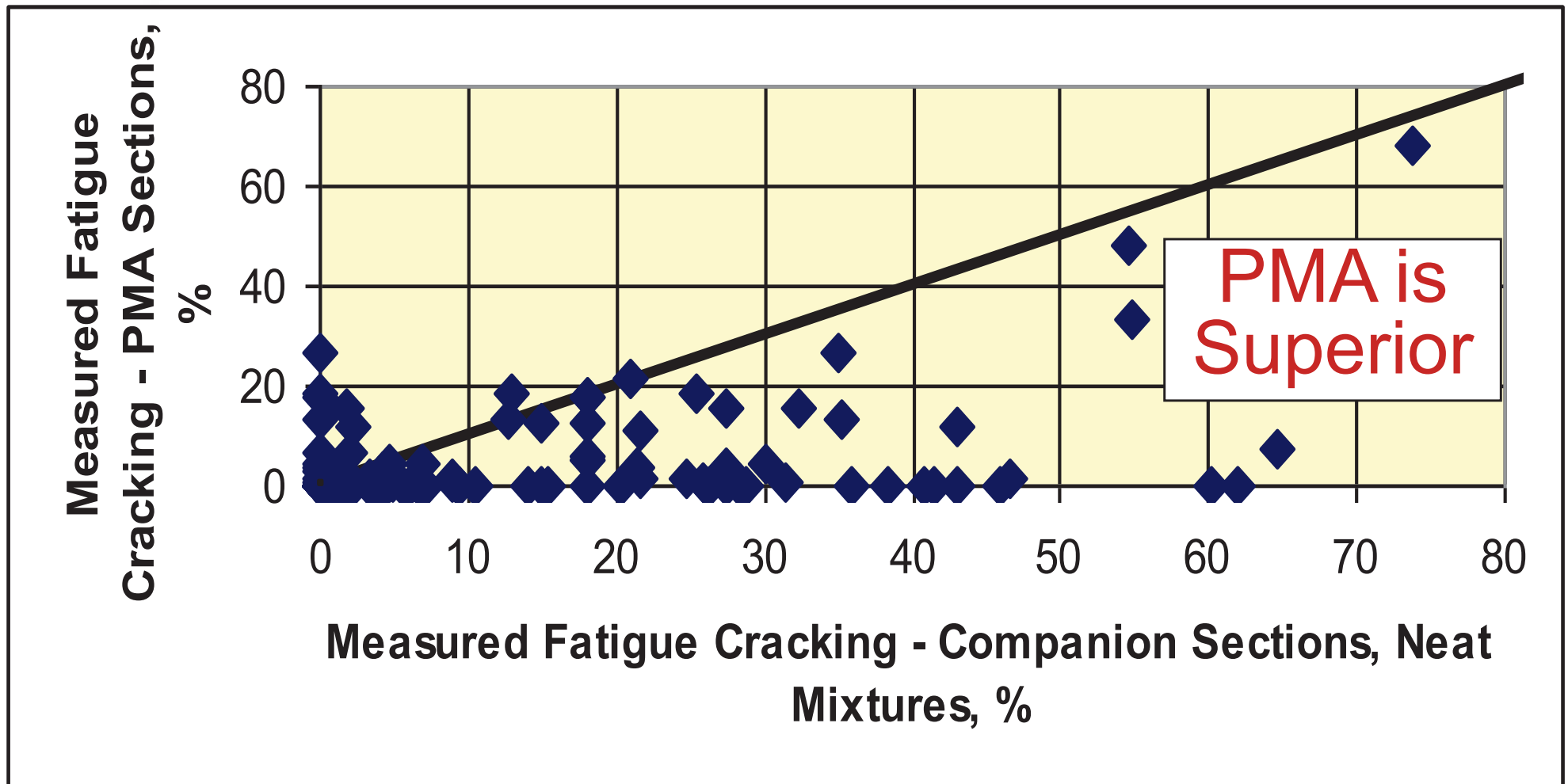


Figure 3 in the report.

Distress Comparison—Transverse Cracking

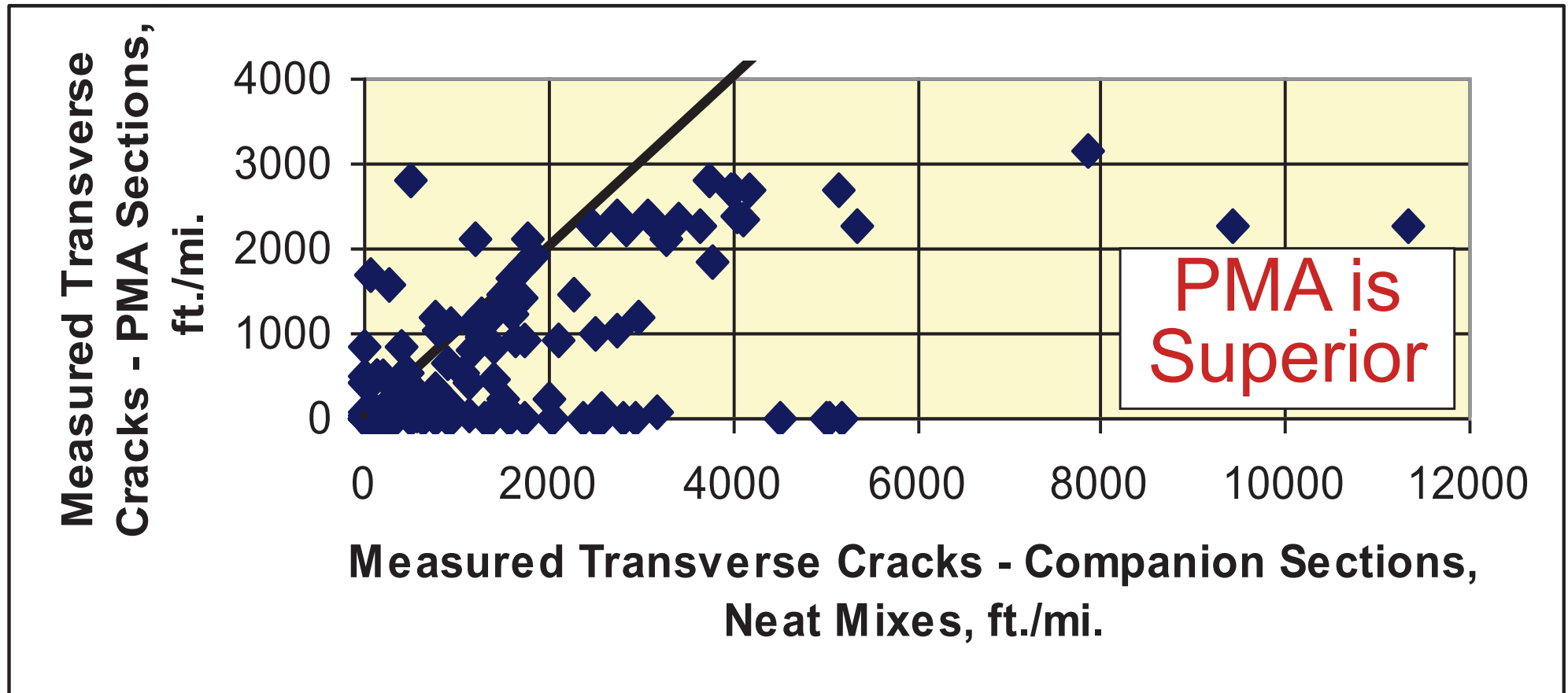


Figure 4 in the report.

Summary of Distress Differences

Distress	Average Difference; Neat Minus PMA Values
Rut Depth, inches	+0.18
Fatigue Cracks, %	+7.1
Transverse Cracks, ft./mi.	+694

Table 1 in the report.

Presentation Overview

1. Introduction
2. Distress Comparison Update
- 3. PMA Calibration Factors & the MEPDG; Version 1.0**
4. Conclusions (Findings & Marketing Issues)

PMA Calibration Factors for Rutting

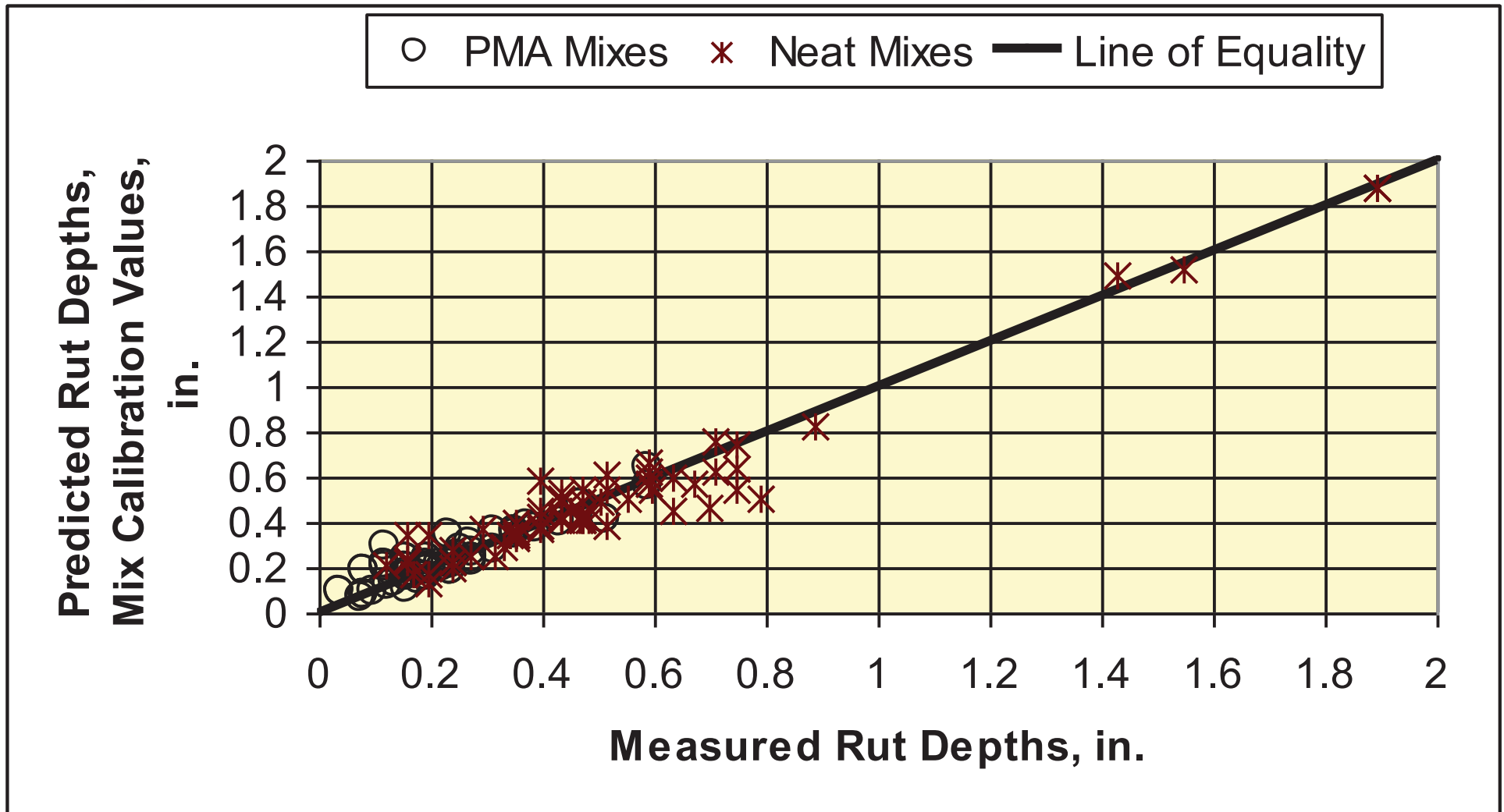
Neat Versus
PMA Mixes

MEPDG Rut Depth Transfer Function

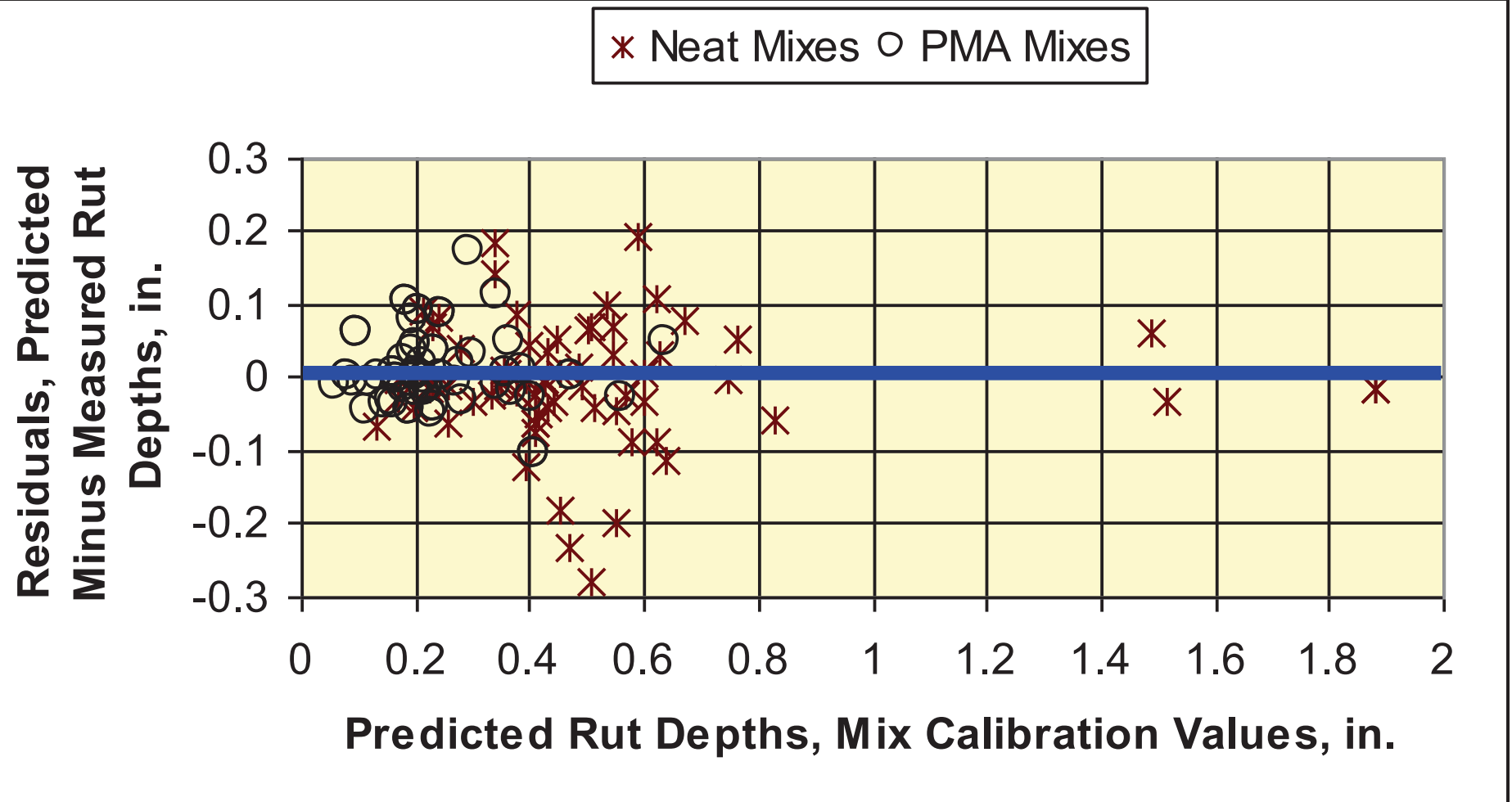
$$\Delta_p \text{ (HMA)} = [h_{HMA} \beta_{1r} k_Z \varepsilon_r \text{ (HMA)}]^* \\ [10^{k_{1r}} N^{k_{2r} \beta_{2r}} T^{k_{3r} \beta_{3r}}]$$

The calibration factor varied in study.

Rutting - Neat versus PMA Sections

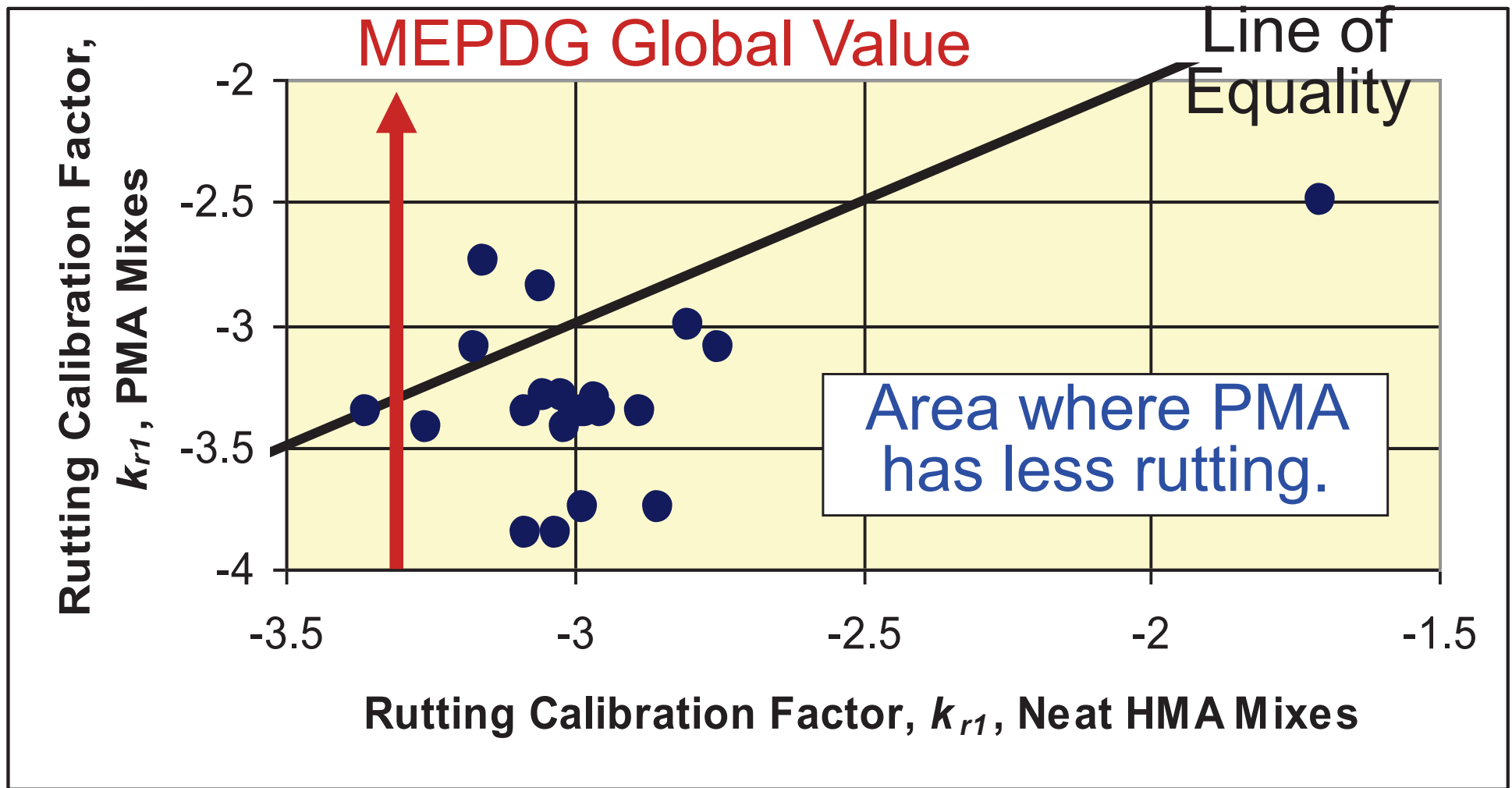


Residuals - Rut Depths

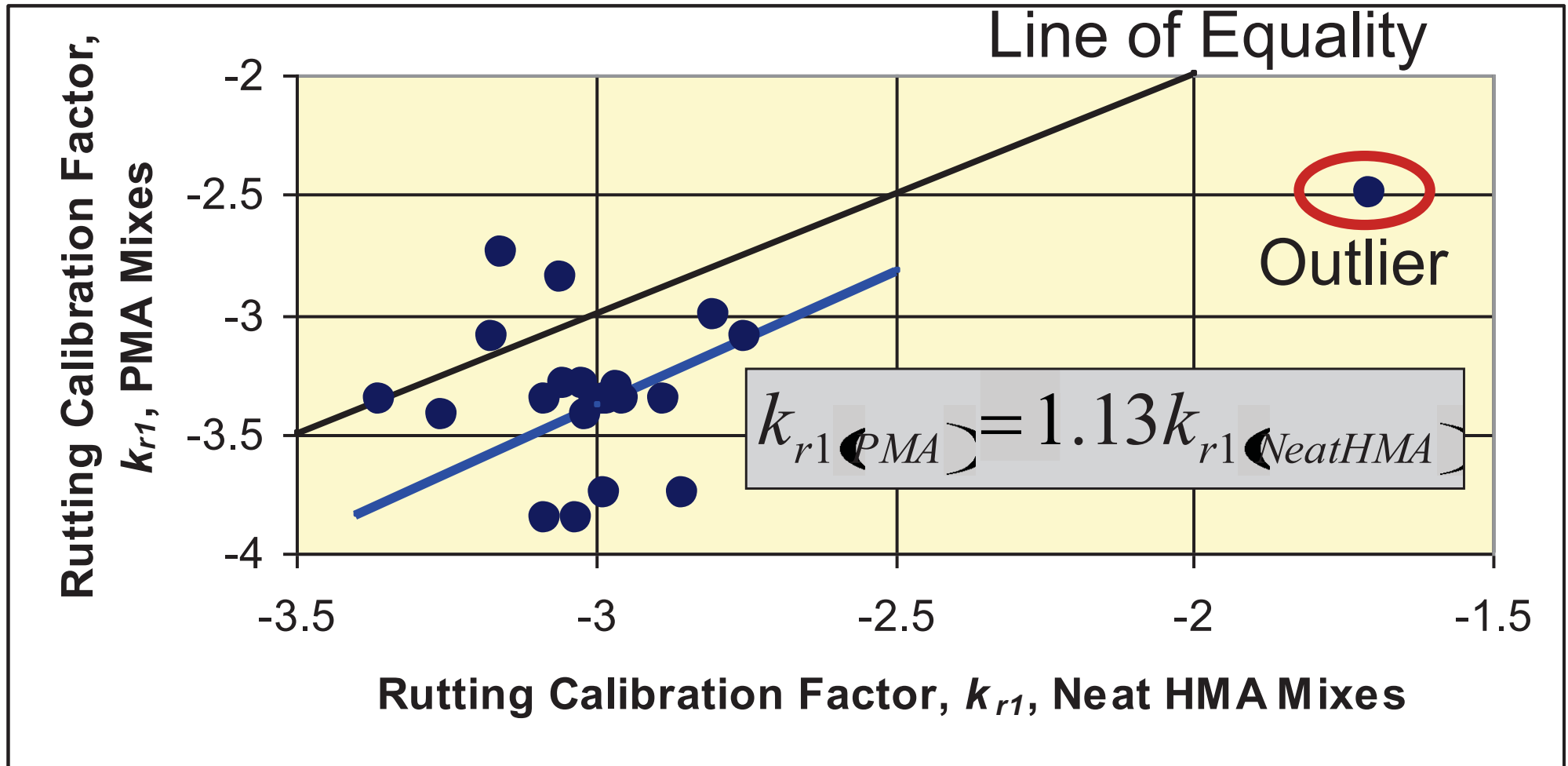


Time does not affect residuals
between neat & PMA mixtures.

Comparison of Neat & PMA Calibration Values: **Rutting**



Comparison of Neat & PMA Calibration Values: **Rutting**



Untitled Mechanistic E...ment Design Guide

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#1

Distress Model Calibration Settings - Flexible New

AC Fatigue AC Rutting Thermal Fatigue Subgrade Rutting AC Cracking CSM Cracking IRI

#2

$$\frac{\epsilon_p}{\epsilon_r} = k_z \beta_{r1} 10^{k_1} T^{k_2 \beta_{r2}} N^{k_3 \beta_{r3}}$$

$$k_z = (C_1 + C_2 * depth) * 0.328196^{depth}$$

$$C_1 = -0.1039 * H_{ac}^2 + 2.4868 * H_{ac} - 17.342$$

$$C_2 = 0.0172 * H_{ac}^2 - 1.7331 * H_{ac} + 27.428$$

Where:
Hac = total AC thickness (in)

#3

NCHRP 1-37A

- ☐ Special Analysis
- ☐ National Calibration
- ☐ State/Regional Calibration
- ☒ Typical Agency Values

#4

K1: -3.35412

K2: 5.5896

K3: 0.479

Br3:

Standard Deviation AC Rutting (RUT): 0.24 * POWER(RUT, 0.8026) + 0.001

Version 1.000

For Help, press F1

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$$k_{r1(PMA)} = 1.13 k_{r1(NeatHMA)}$$

PMA Calibration Factors for Fatigue Cracking

Neat Versus
PMA Mixes

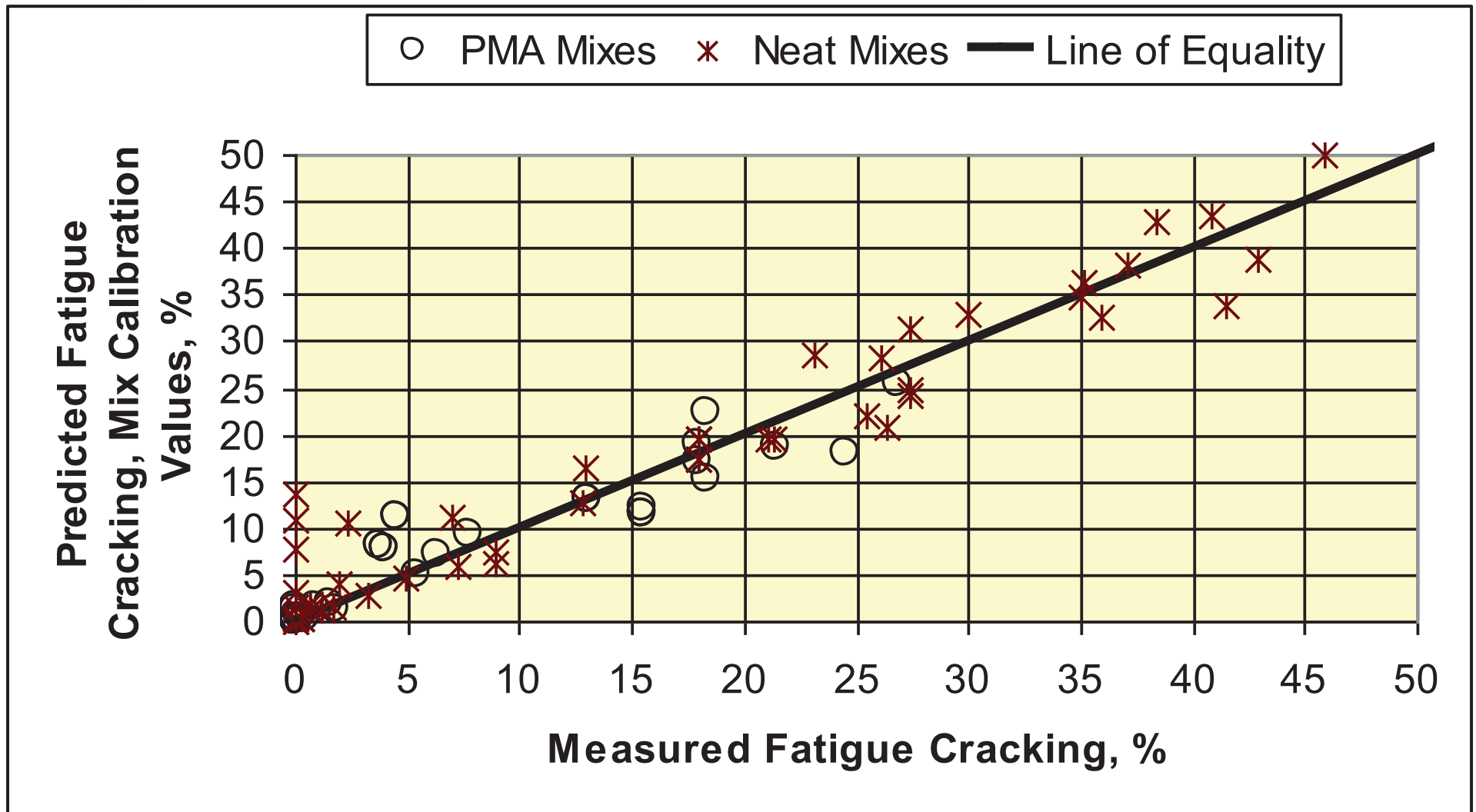
MEPDG Fatigue Cracking Transfer Function

$$N_f = k_{1f} 10^M C_H \beta_{1f} \epsilon_t^{k_{2f} \beta_{2f}} E_{HMA}^{k_{3f} \beta_{3f}}$$

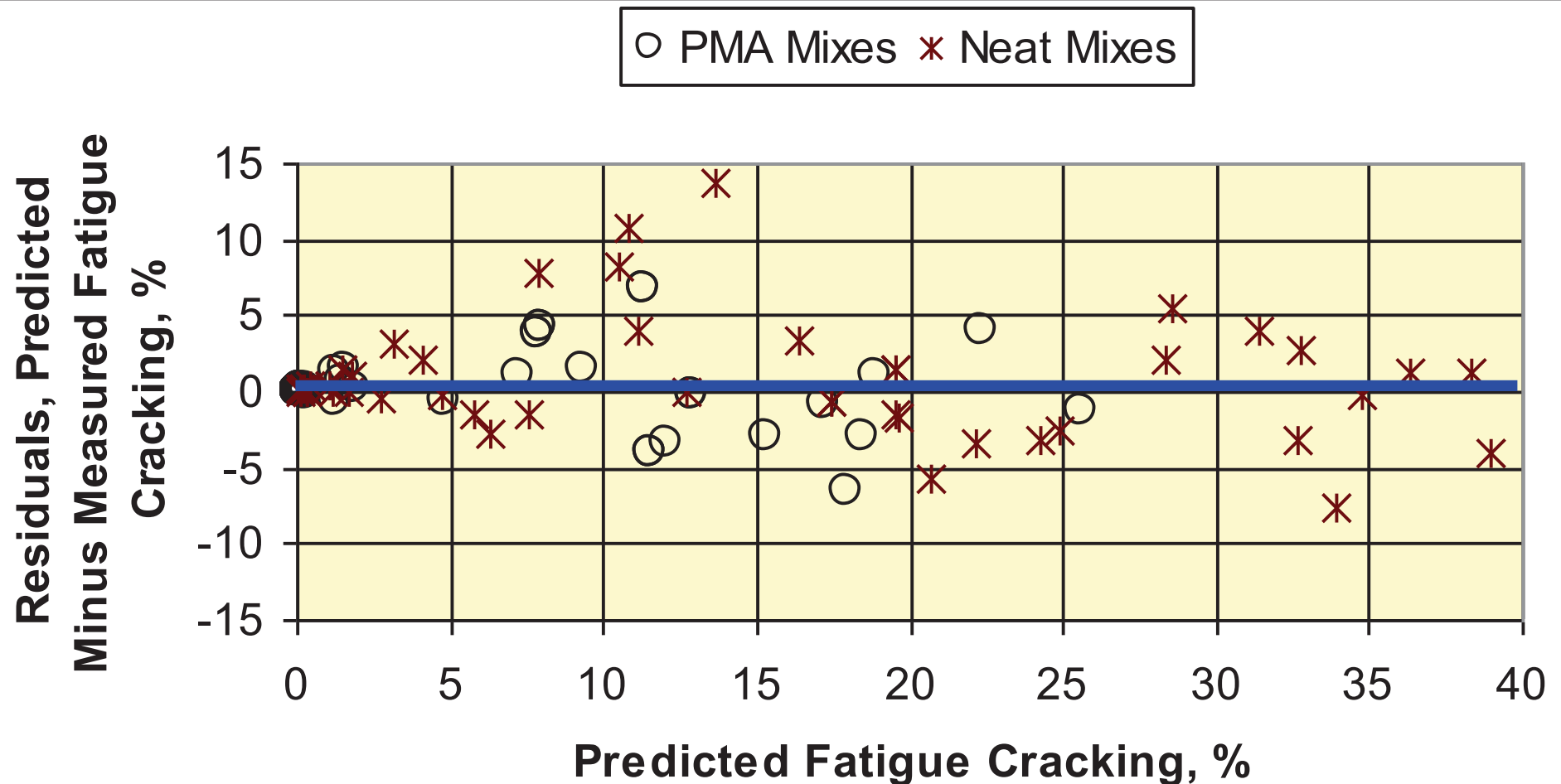
The calibration factor varied in study.

$$FC_{Bottom} = \left(\frac{1}{60} \right) \left(\frac{C_4}{1 + e^{C_1 C_1^* + C_2 C_2^* \log \left(DI_{Bottom} * 100 \right)}} \right)$$

Fatigue Cracking - Neat versus PMA Sections

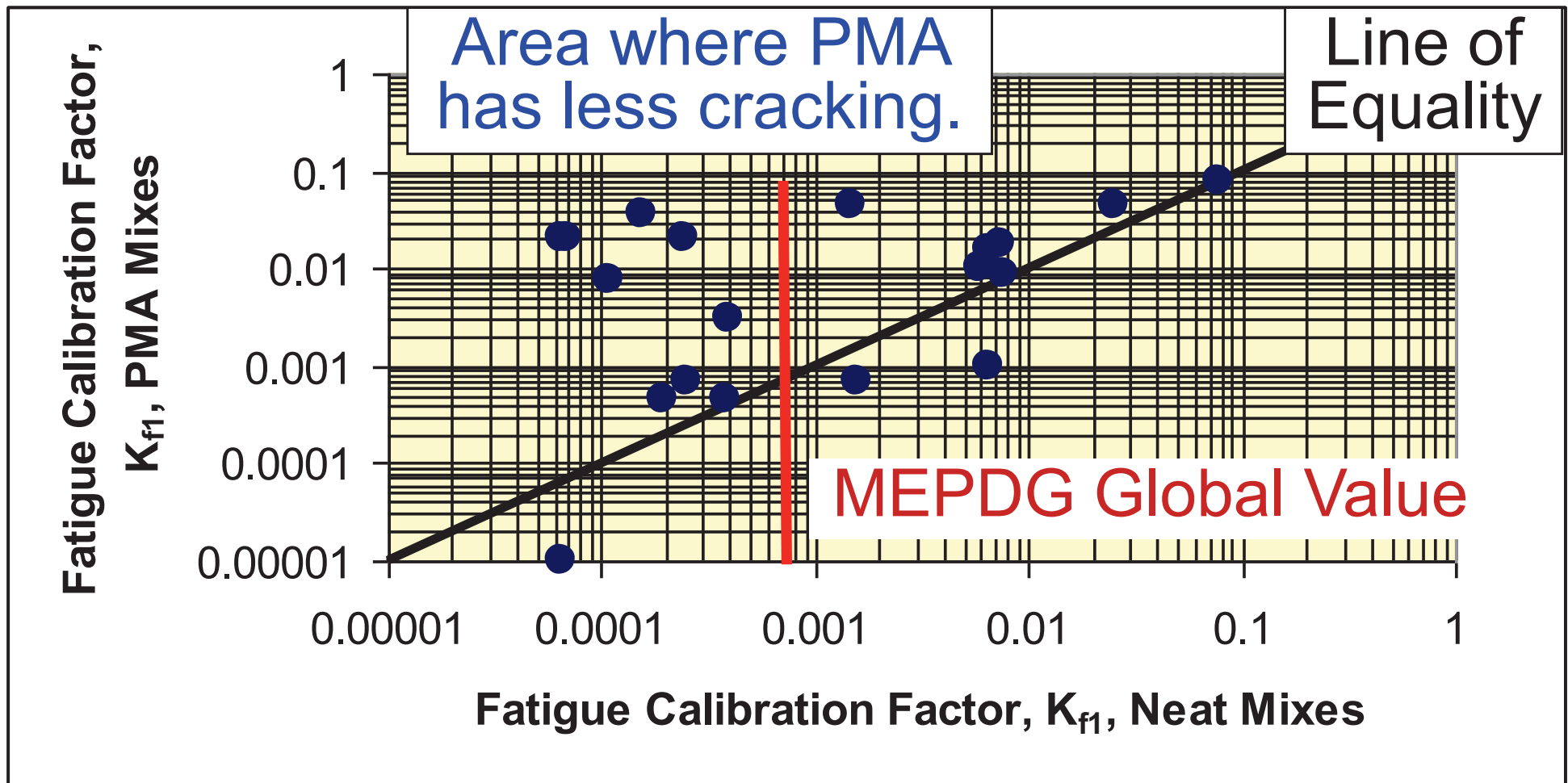


Residuals - Fatigue Cracking

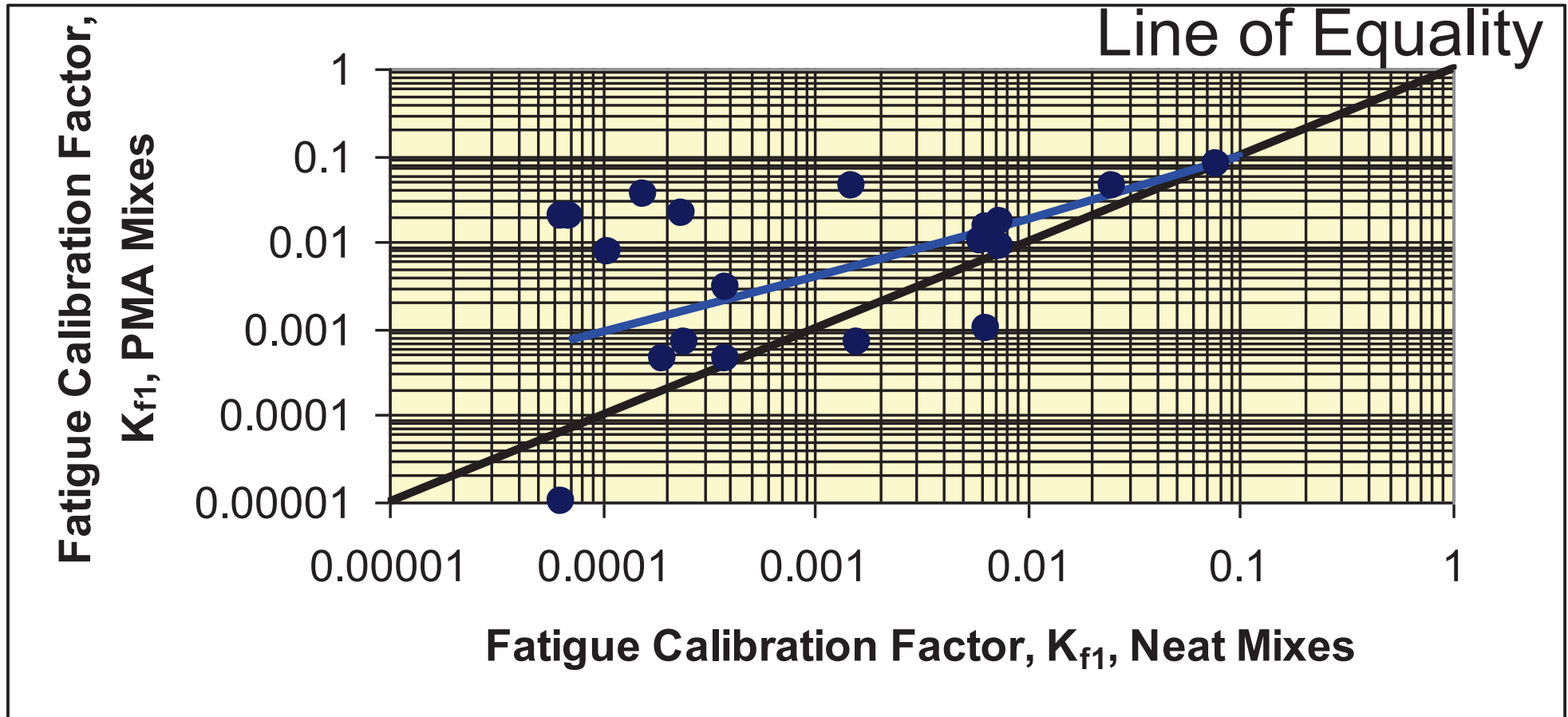


Variability in measured distress causing higher dispersion.

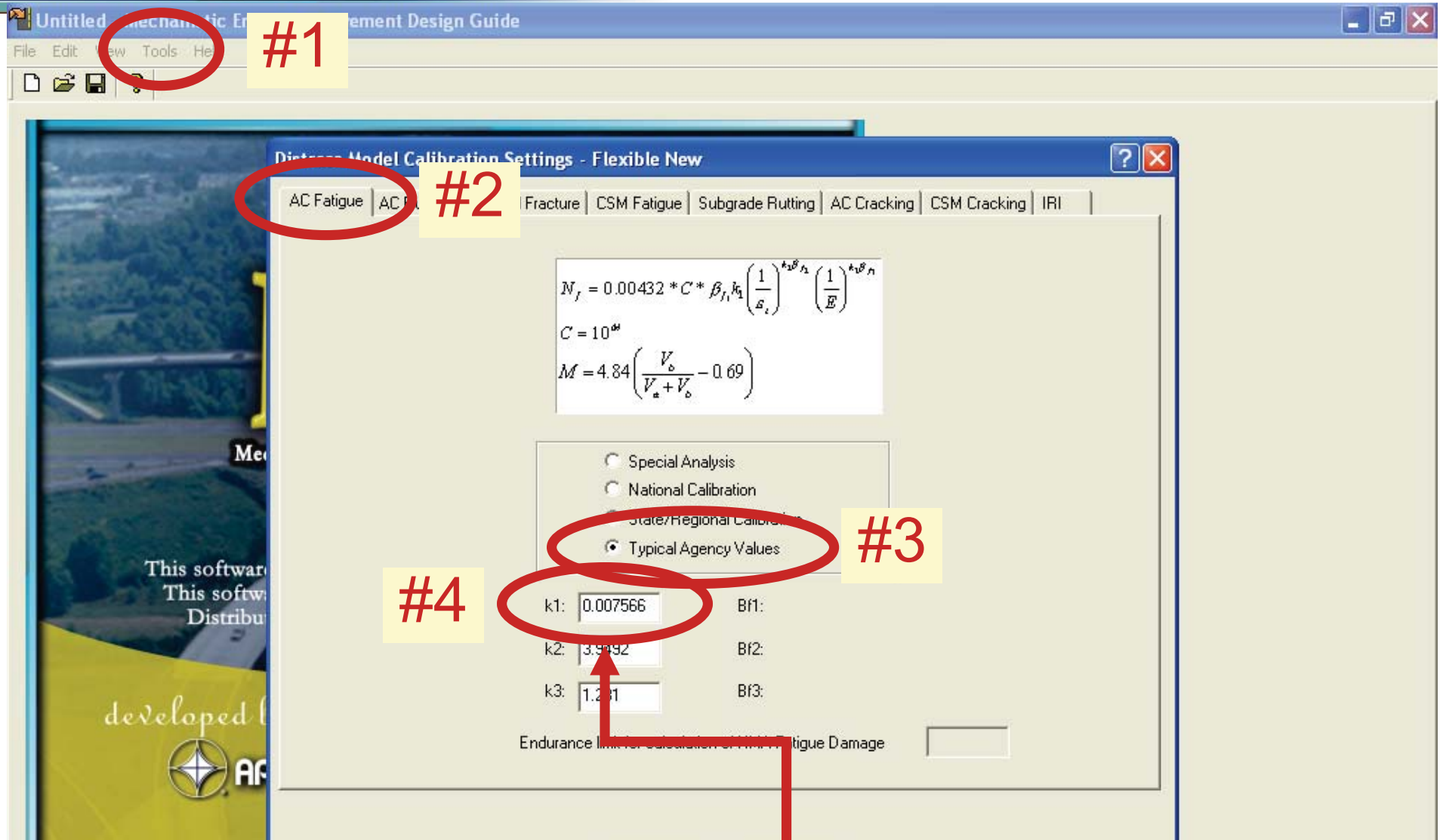
Comparison of Neat & PMA Calibration Values; **Fatigue**



Comparison of Neat & PMA Calibration Values; **Fatigue**



$$k_{f1(PMA)} = 10^{-\left(\text{Log } k_{f1(NeatHMA)}\right)^{0.8}}$$



$$k_{f1(PMA)} = 10^{-\left(\text{Log } k_{f1(NeatHMA)} \right)^{0.8}}$$

PMA Calibration Factors for Transverse Cracking

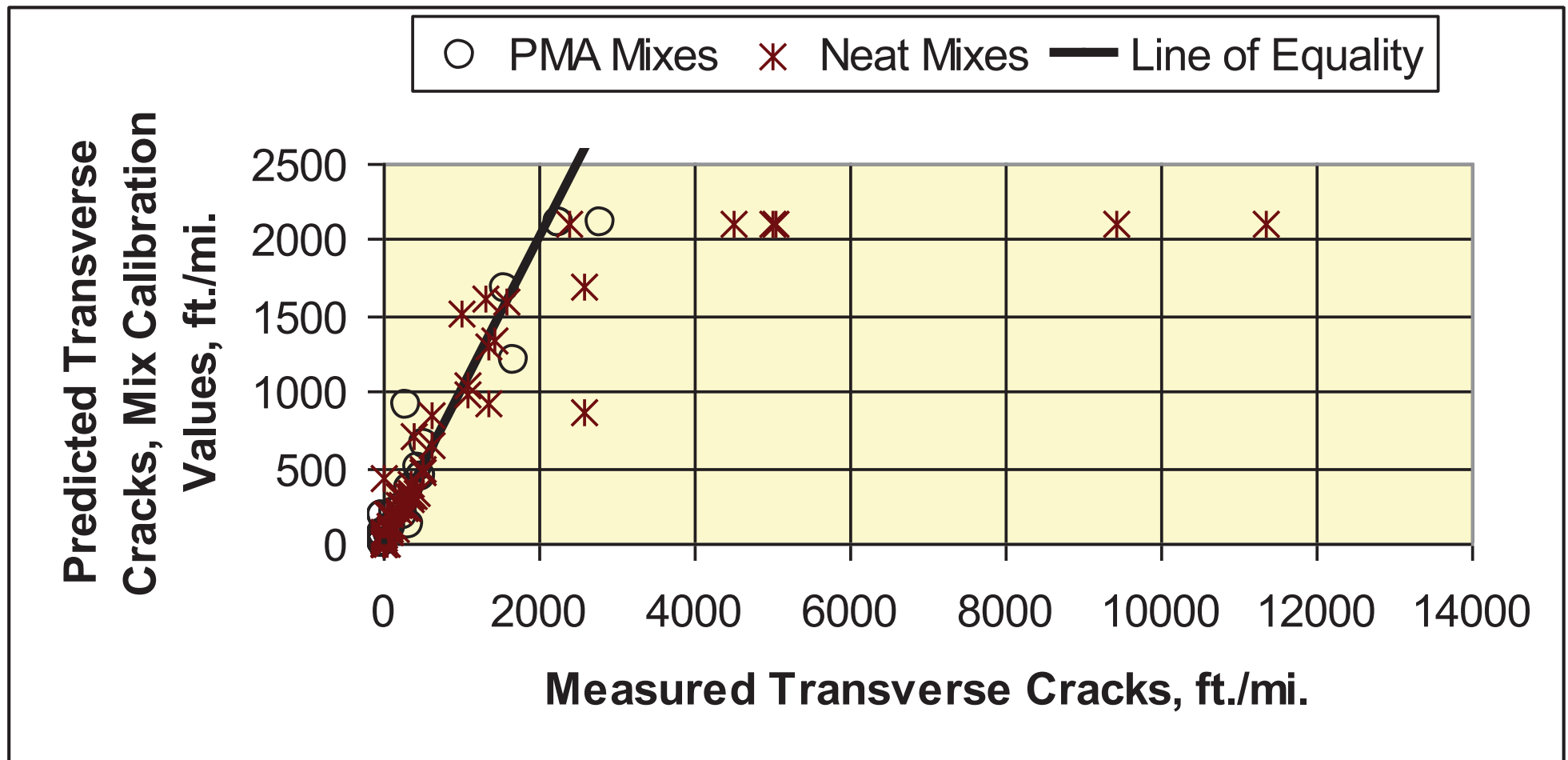
**Neat Versus
PMA Mixes**

MEPDG Transverse Cracking Transfer Function

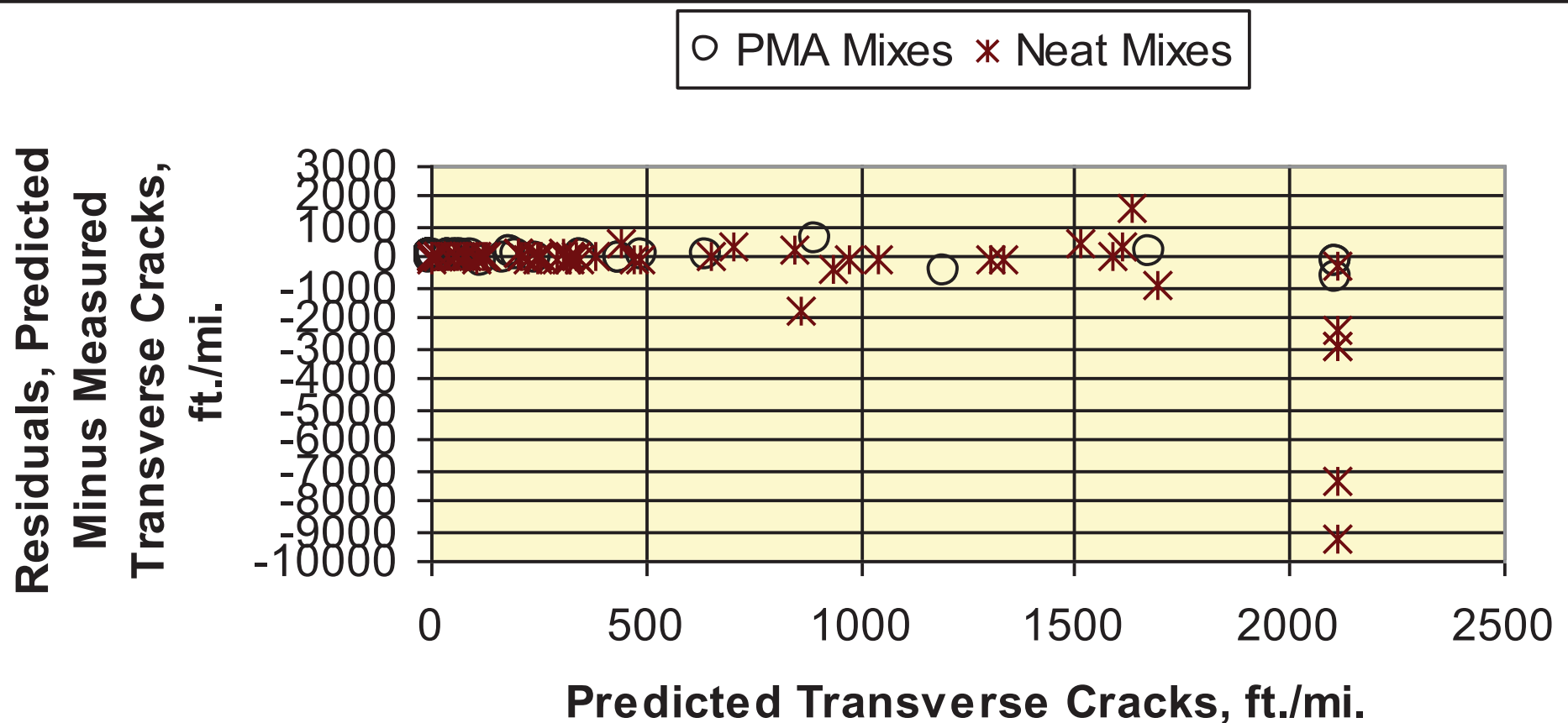
$$TC = \beta_t N \left[\frac{1}{\sigma_d} \text{Log} \left(\frac{C_d}{H_{HMA}} \right) \right]$$

The calibration factor varied in study.

Transverse Cracking - Neat versus PMA Sections

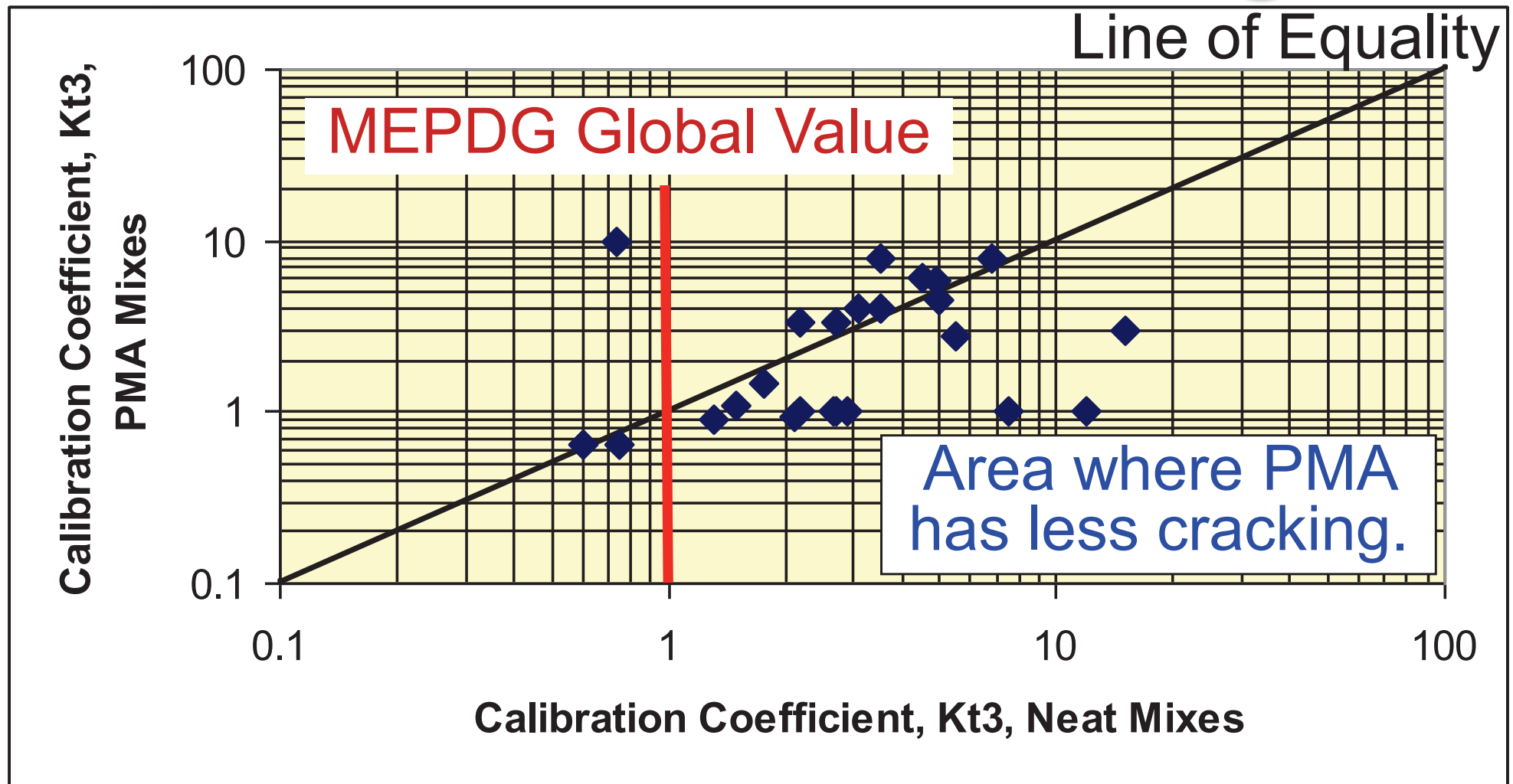


Residuals - Transverse Cracking

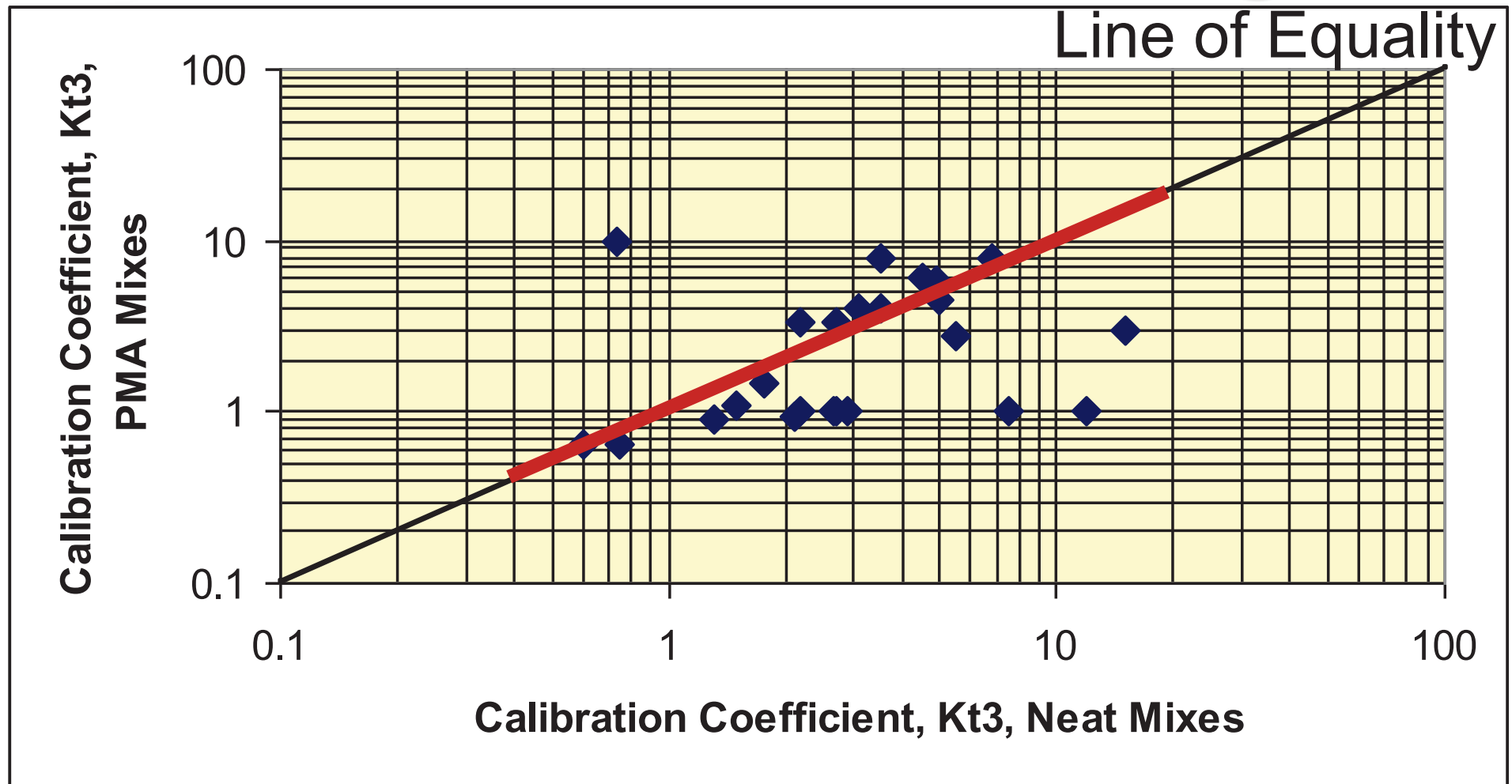


Negative bias caused by limit of predicted transverse cracks, 2110 ft./mi.

Comparison of Neat & PMA Calibration Values; **Transverse Cracking**



Comparison of Neat & PMA Calibration Values; **Transverse Cracking**



$$\beta_{t3} [PMA] = \beta_{t3} [NeatHMA]$$

Untitled - Mechanistic Empirical Pavement Design Guide

File Edit View Tools Help

#1

Distress Model Calibration Settings - Flexible New

#2

AC Rutting Thermal Fracture CSM Fatigue Subgrade Rutting AC Cracking CSM Cracking IRI

$$C_f = 400 * N\left(\frac{\log C / h_{ac}}{\sigma}\right)$$

$$\Delta C = (k * \beta_t)^{n+1} * A * \Delta K^n$$

$$A = 10^{(4.389 - 2.52 * \log(E * \sigma_m * n))}$$

Cr = observed amount of thermal cracking (ft/500 ft)
 k = regression coefficient determined through field calibration
 N() = standard normal distribution evaluated at ()
 σ = standard deviation of the log of the depth of cracks in the pavements
 C = crack depth (in)
 h_{ac} = thickness of asphalt layer (in)
 ΔC = Change in the crack depth due to a cooling cycle.
 ΔK = Change in the stress intensity factor due to a cooling cycle.
 A, n = Fracture parameters for the asphalt mixture.
 E = Mixture stiffness.
 σ_m = Undamaged mixture tensile strength.
 β_t = Calibration parameter.

☐ Special Analysis
☐ National Calibration
☒ State/Regional Calibration

#3

Level 1 K: 1.5 Bt1: 1 Std. Dev. (THERMAL): 0.1468 * THERMAL + 65.027

Level 2 K: 0.5 Bt2: 1 Std. Dev. (THERMAL): 0.2841 * THERMAL + 55.462

Level #4 Bt3: 1 Std. Dev. (THERMAL): 0.3972 * THERMAL + 20.422

OK Cancel

Version 1.000

For Help, press F1

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$$\beta_{t3(PMA)} = \beta_{t3(NeatHMA)}$$

Example Comparison; Rutting

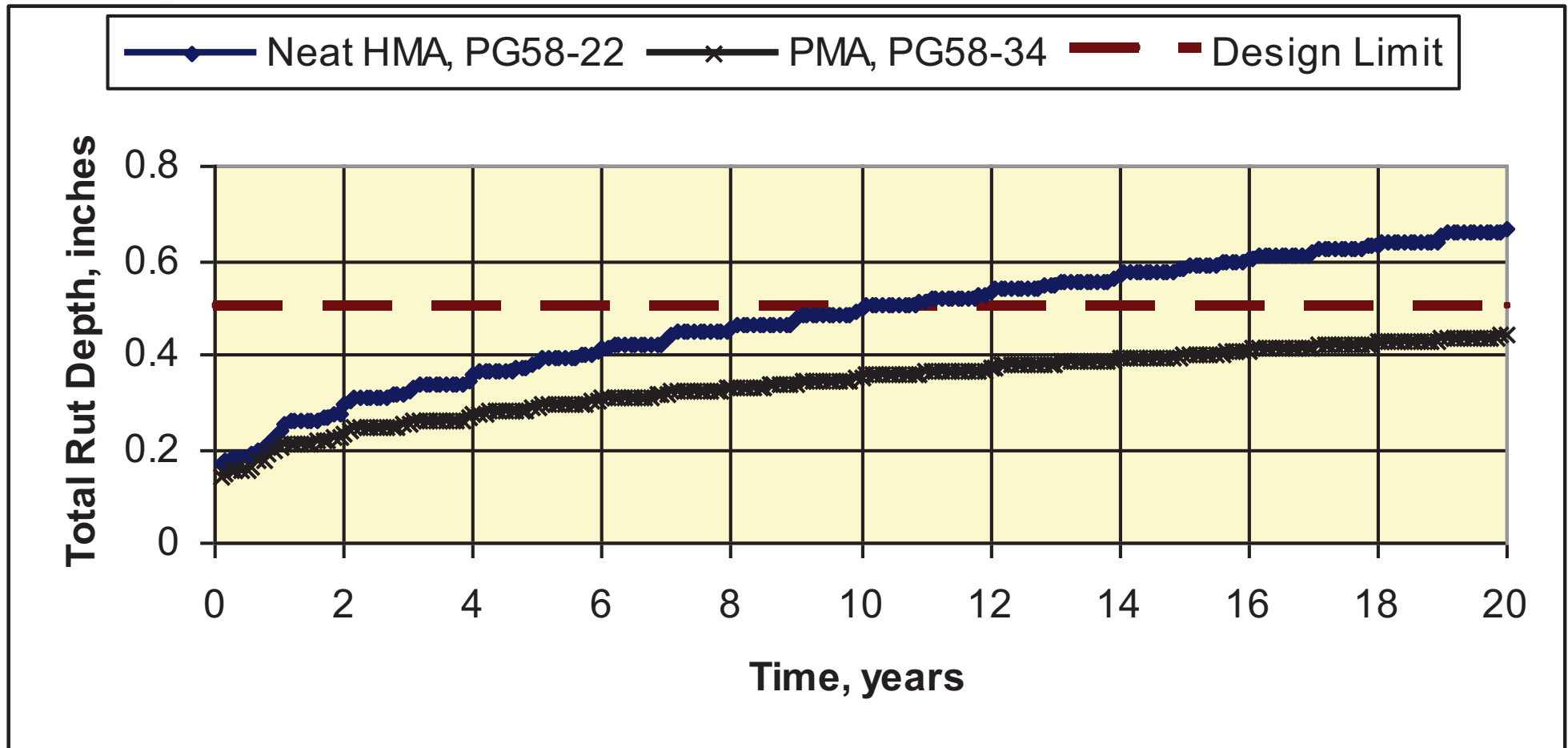


Figure 17 in the report.

Example Comparison: Fatigue Cracking

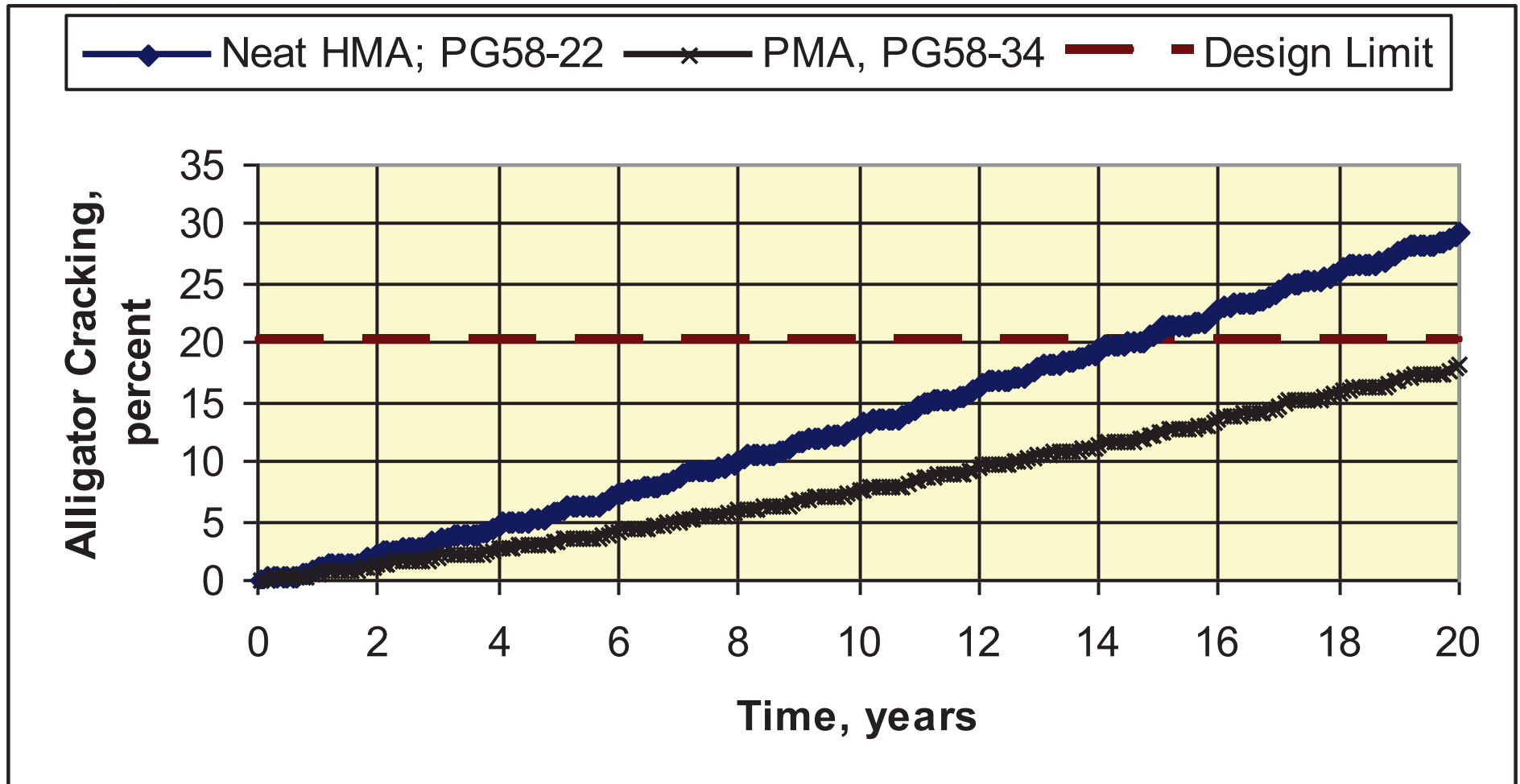


Figure 18 in the report.

Example Comparison; Thermal Cracking

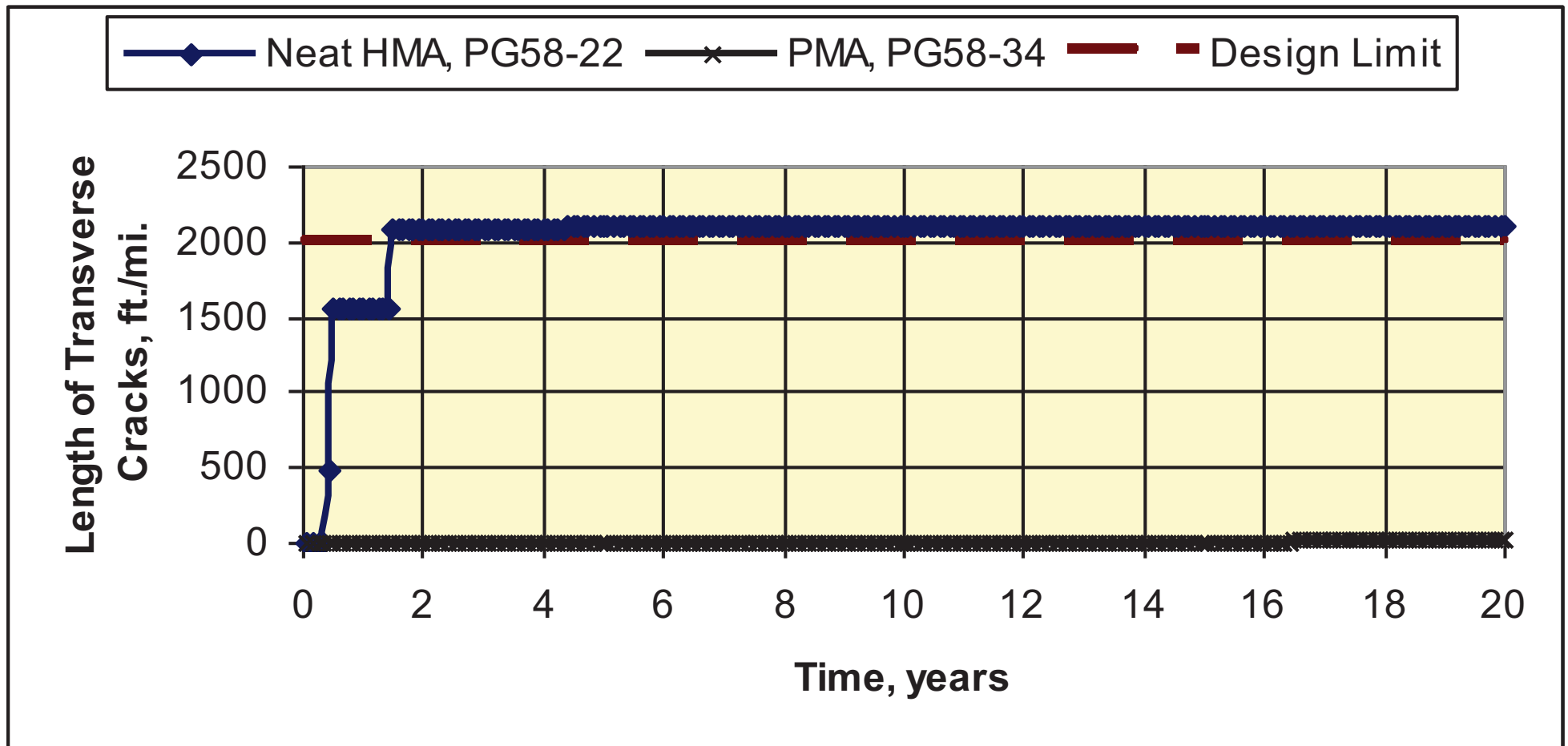


Figure 19 in the report.

Example Comparison; Roughness

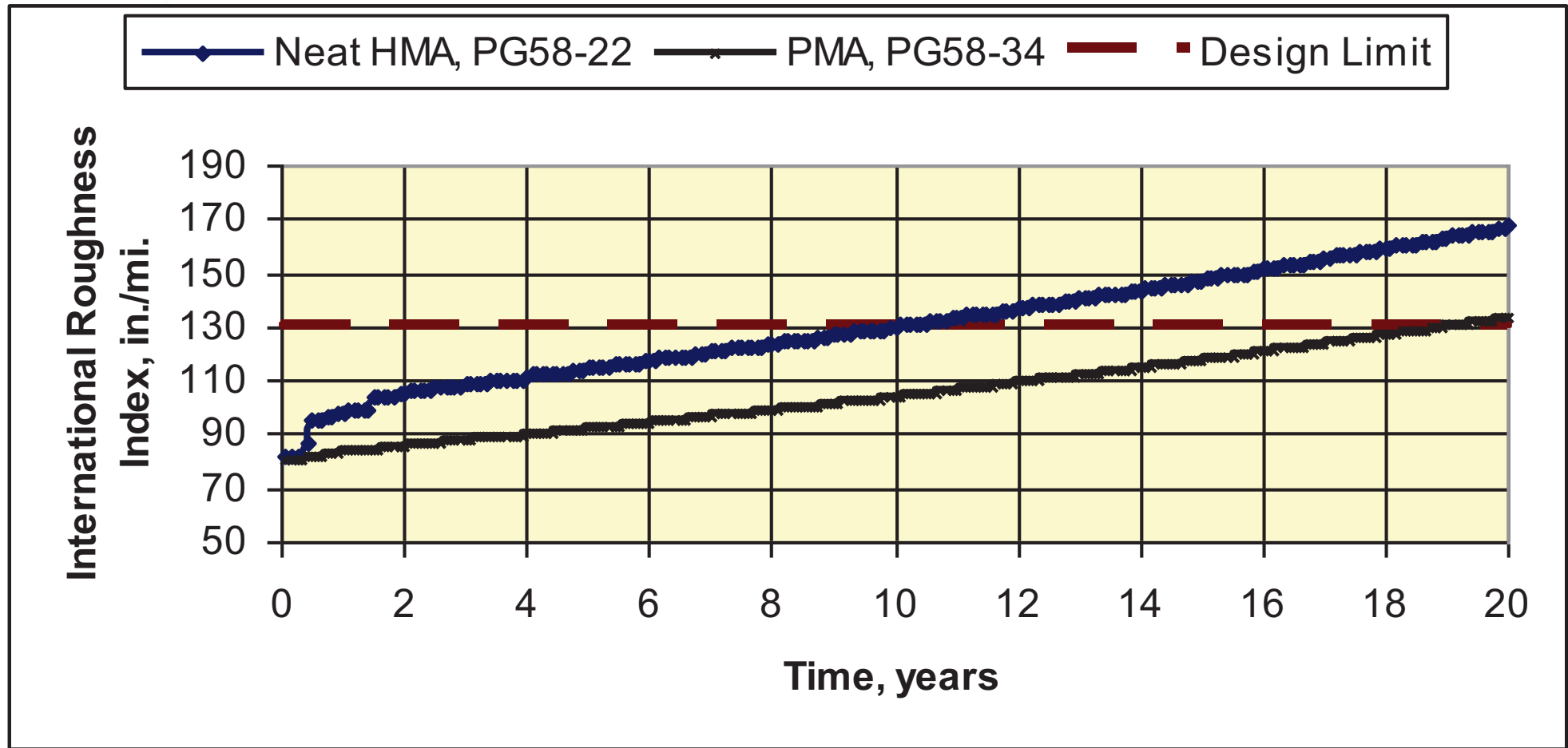


Figure 20 in the report.

Presentation Overview

1. Introduction
2. Distress Comparison Update
3. PMA Calibration Factors & the MEPDG
- 4. Conclusions (Findings & Marketing Issues)**

Findings

- **Rutting** – K_{1r} for PMA mixtures **is lower** than for neat HMA mixtures.
- **Fatigue Cracking** – K_{1f} for PMA mixtures **is greater** than for neat HMA mixtures.
- **Transverse Cracking** – B_{t3} for PMA mixtures **is the same** as for neat HMA mixtures.

Marketing Issue

- Rutting & Transverse Cracks:
 - Controls HMA properties
 - Does not control HMA thickness
- Fatigue Cracks:
 - Controls HMA thickness
 - Less control over HMA properties

Marketing Issue

- PMA mixes—Less distress over neat HMA mixes.
- High volume roadways—Thinner PMA layers can be used.
- Low volume roadways—Pavement over weak foundations, overlays of severely distressed pavements – **DO NOT DECREASE HMA THICKNESS.**

Marketing Issue

- **For LCCA** – increase service life for PMA mixtures (rutting, transverse cracks, & fatigue cracks)
- **For design** – reduce HMA layer thickness for PMA mixtures (fatigue cracks)
- **BUT, inappropriate to apply both findings.**

Recommendation

- DECREASING THE PAVEMENT THICKNESS IS A SHORT TERM BENEFIT!
- DO **NOT** DECREASE THICKNESS OF PMA LAYERS AND PAVEMENT STRUCTURE.
- TAKE THE INCREASE IN SERVICE LIFE FOR LCC ANALYSES.

**Thank you for your attention -
Any questions?**



Study Sponsors

Industry Associations

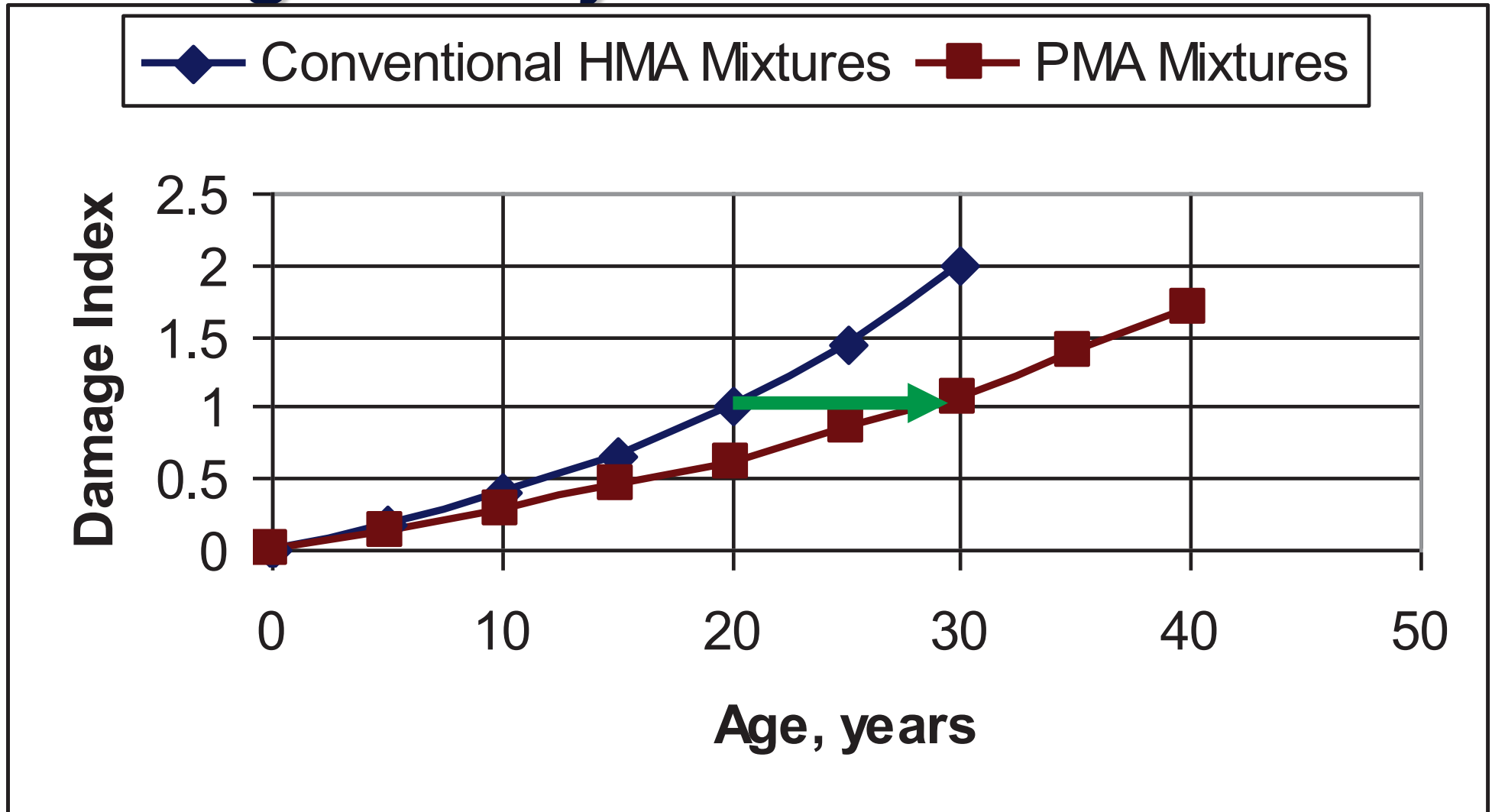
- The Asphalt Institute
- The Association of Modified Asphalt Producers

Federal Highway Administration

Corporate Sponsors

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- ATOFINA Petrochemicals, Inc.
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- Dynasol LLC
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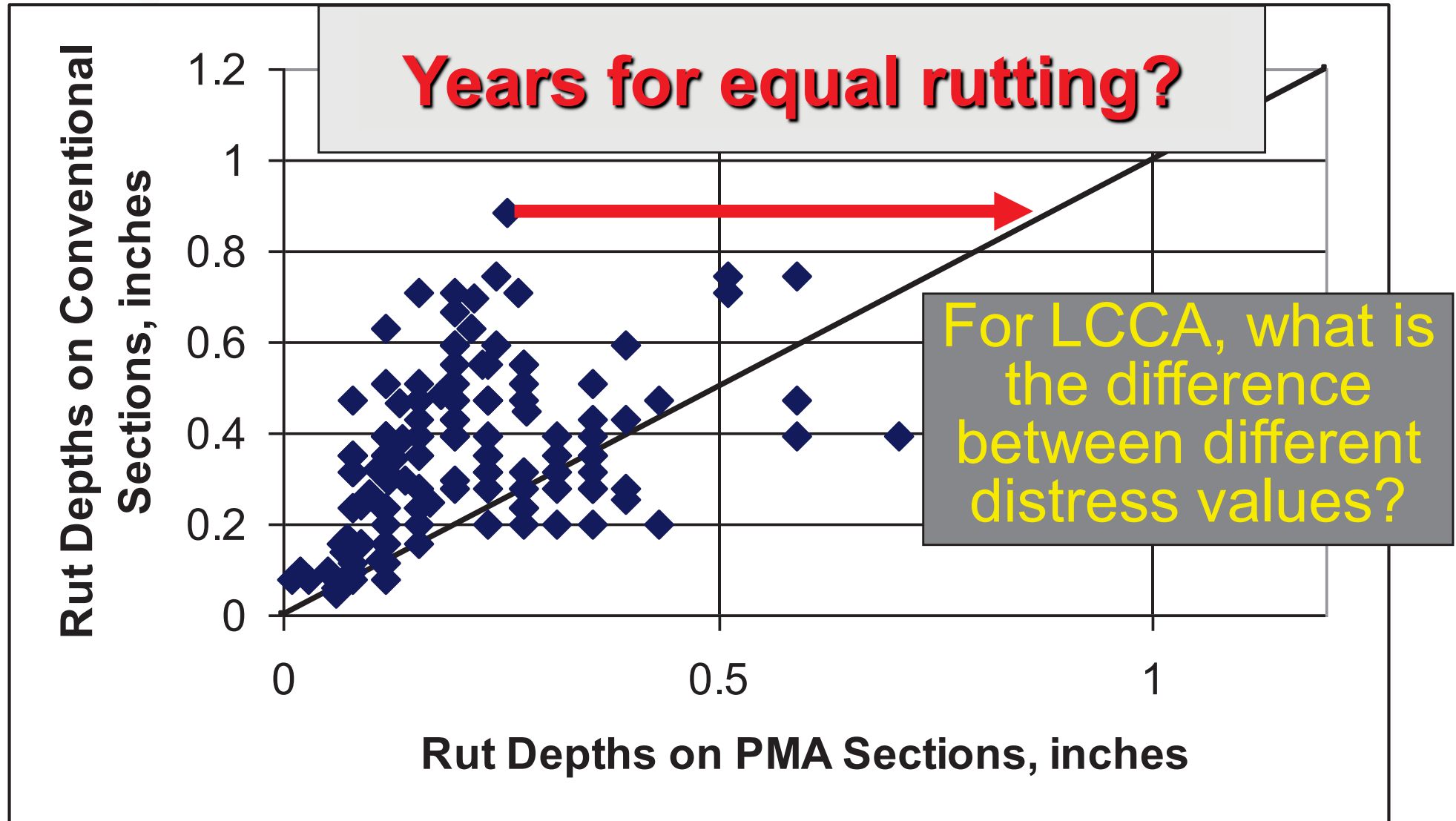
Enhanced Performance Based on Damage Analysis



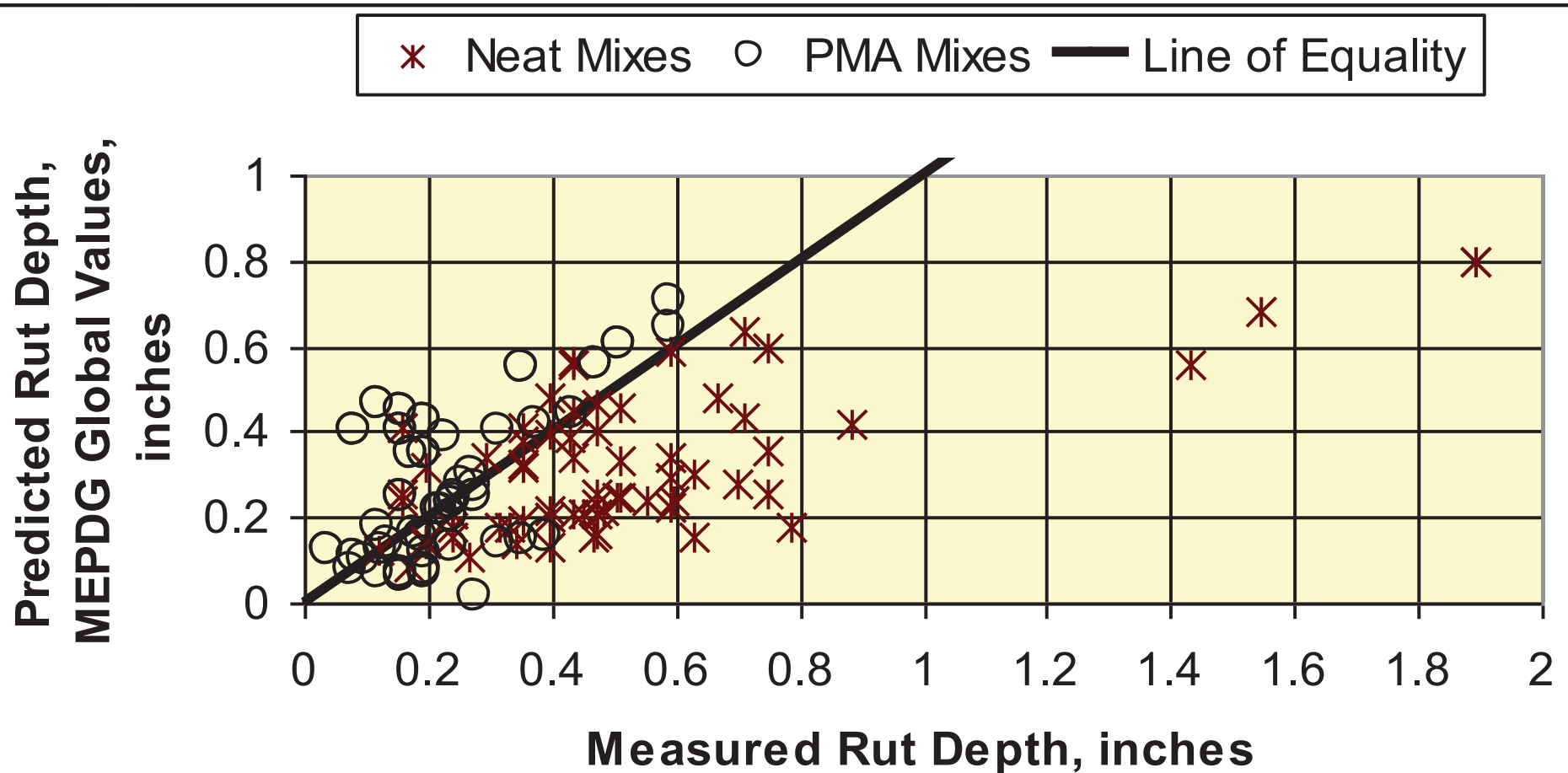
Number of Test Sections - Experimental Factorial

Type of Pavement Structure	Segments with PMA Mixtures
Conventional	17
Deep-Strength	14
Full-Depth	10
HMA over HMA	14
HMA over PCC	15

Quantifying the Effects of PMA

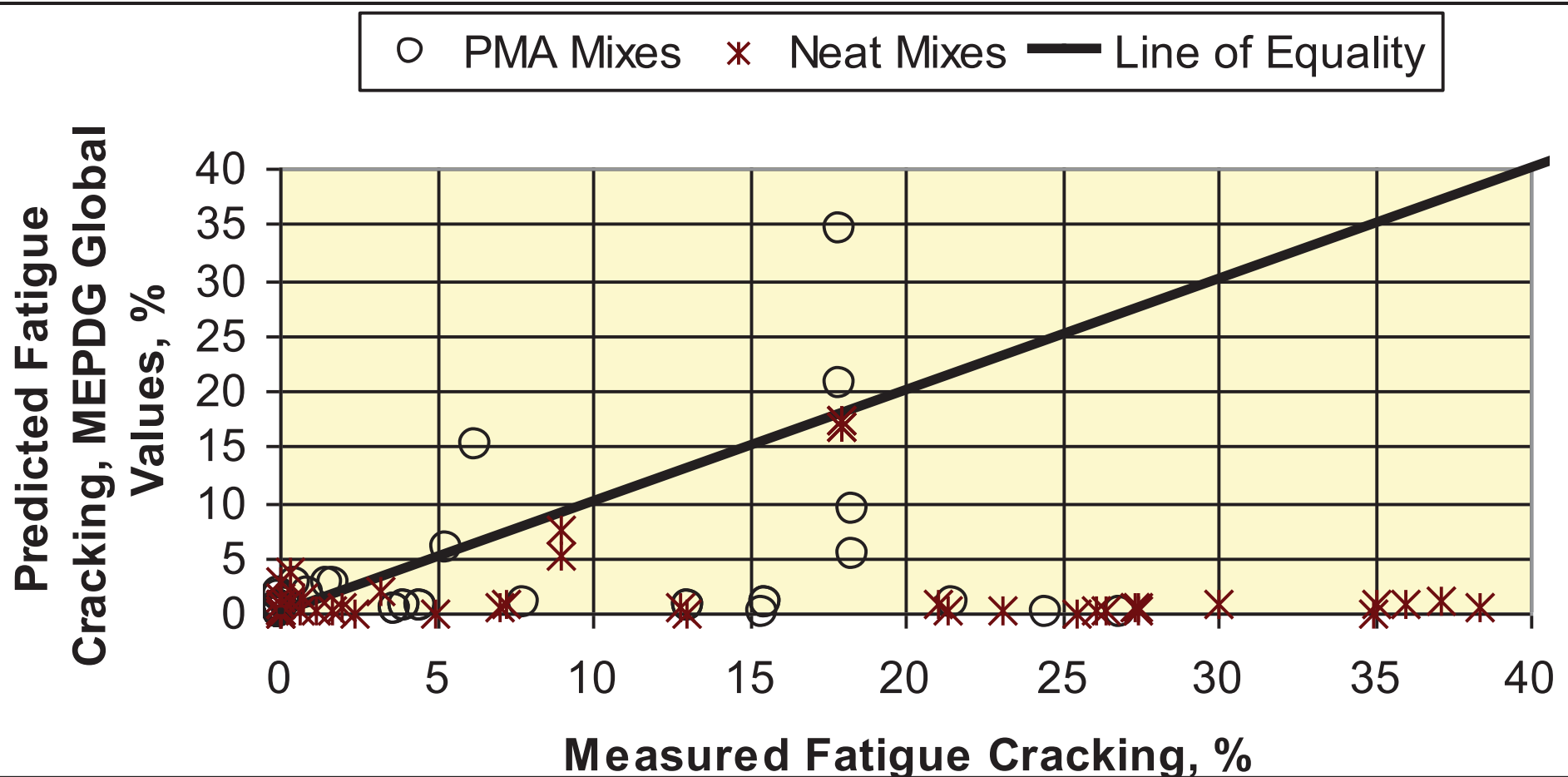


Predicted Rutting Using MEPDG Global Values



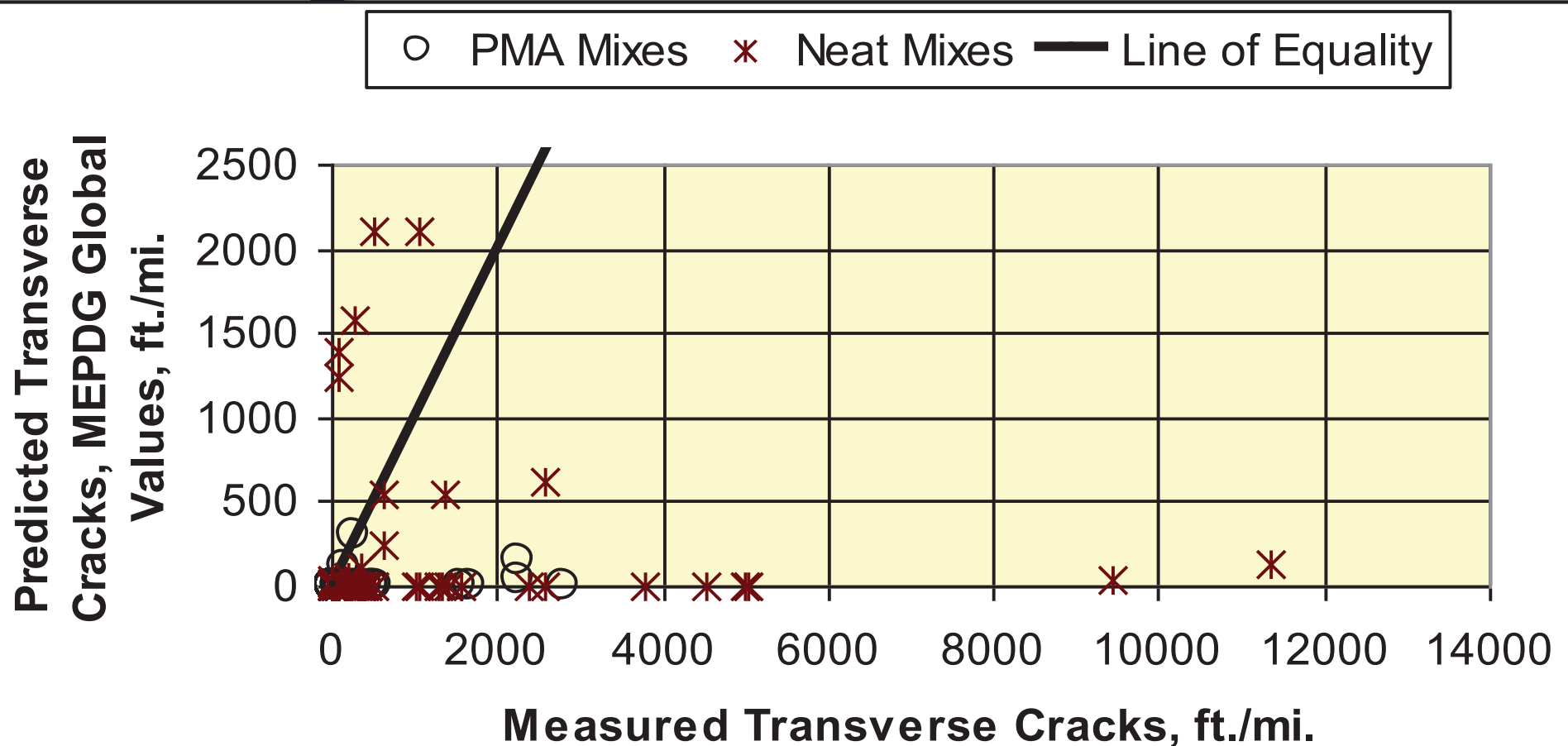
MEPDG global calibration factors for rutting.

Predicted Fatigue Cracking Using MEPDG Global Values



MEPDG global calibration factors for fatigue cracks.

Predicted Transverse Cracking Using MEPDG Global Values



MEPDG global calibration factors for transverse cracks.

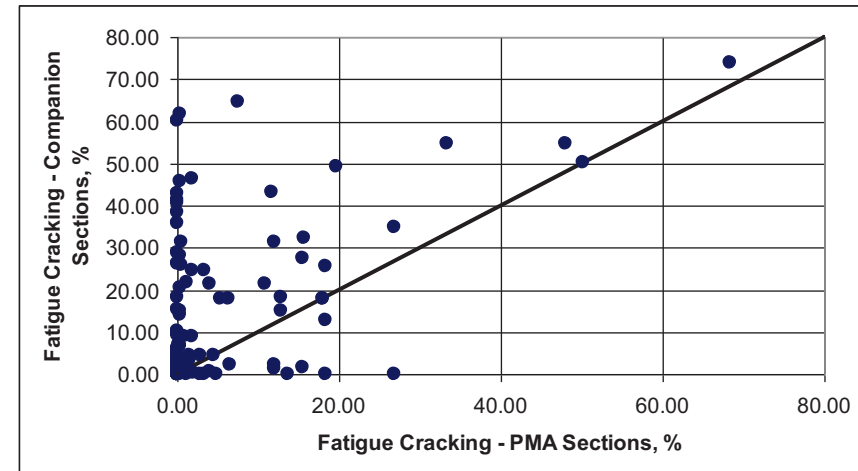
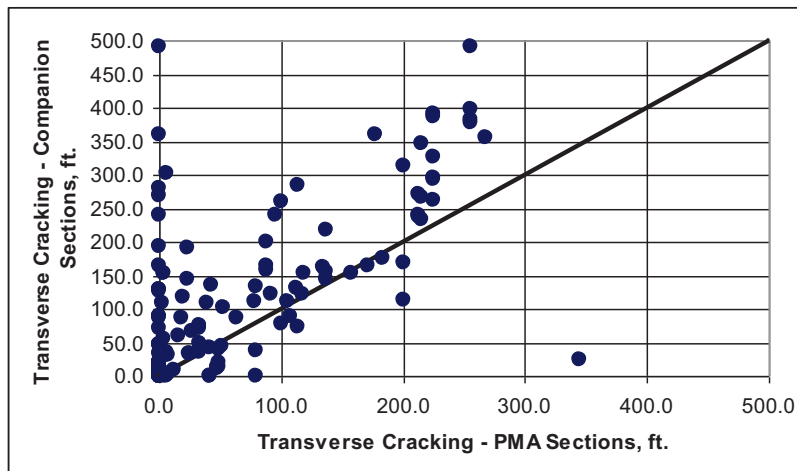
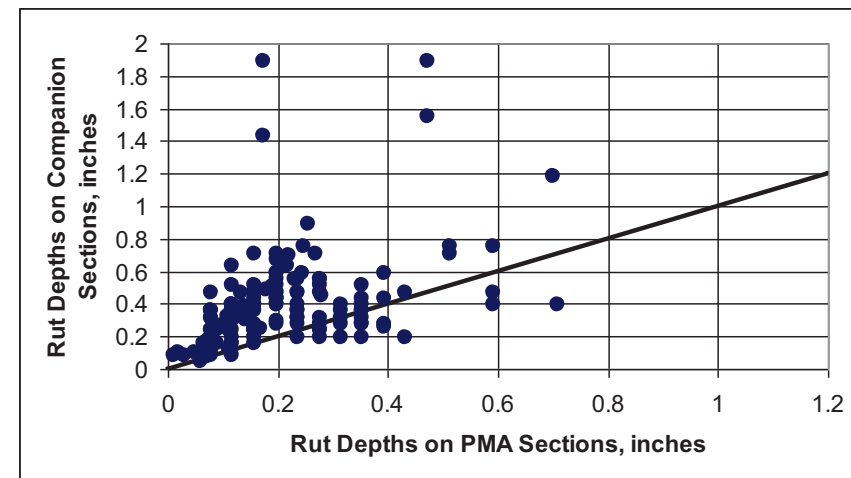
Summary of Measured Distress Comparisons

PMA sections have:

- 1. *Less rutting***; difference not related to time & traffic.
- 2. *Less fatigue cracks***; difference not related to time & traffic.
- 3. *Less transverse cracks***; difference increases with time.

Findings

- Use of PMA reduces distress in pavements & overlays
 - Less Fatigue Cracking
 - Fewer Transverse Cracks
 - Smaller Ruts



Findings

- Analysis using MEPDG version 1.0 confirms need for different calibration factors for predicting performance of PMA mixtures.

