

# **Development of A High Temperature Performance Based Binder Specification**

# Problem-High Temperature Binder Criteria

- Does  $G^*/\sin\delta$  reflect rutting performance of modified binders.
  - General anecdotal data says no.
- What are the alternatives?
  - ZSV, LSV, Creep & Recovery testing

# High Temperature Binder Criteria

- What is Rutting?
  - Rutting is the plastic deformation of a mix caused by heavy traffic loads.
  - This is a high strain failure in the pavement. It is a non-linear response.
  - Linear criteria of the binder are not likely to correlate with failure.



# High Temperature Binder Criteria

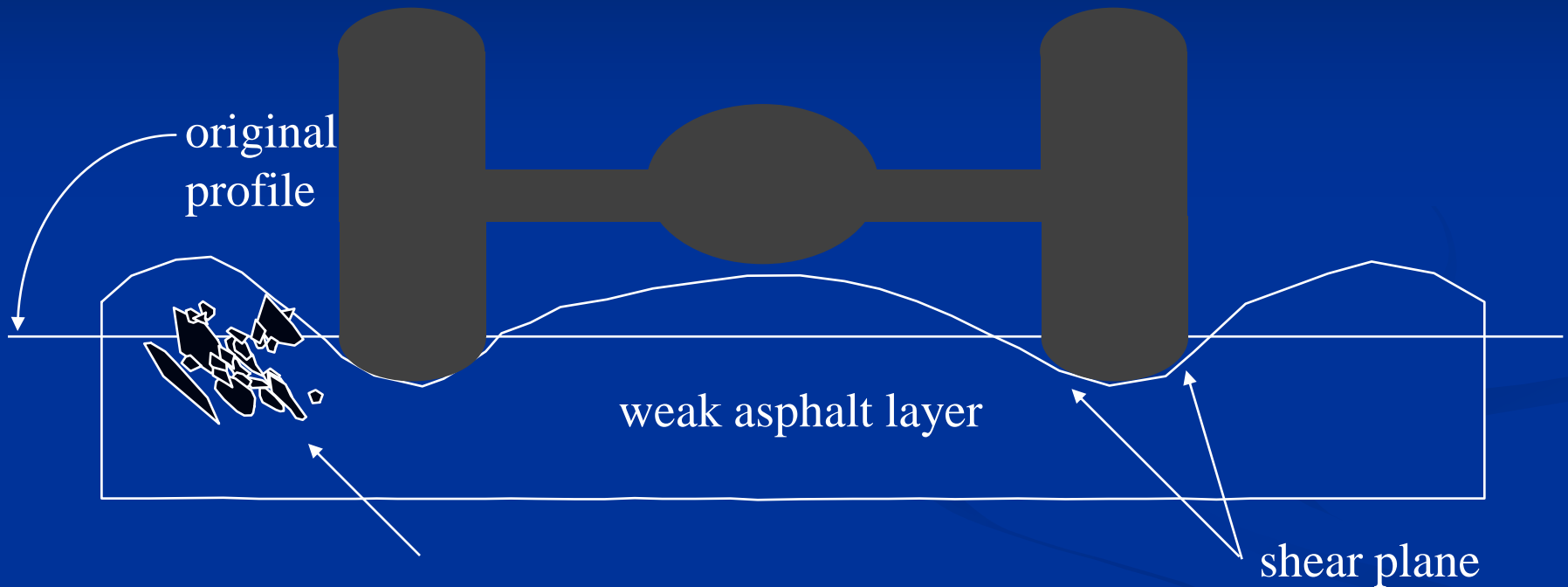
- Current spec,  $G^*$  and  $\delta$  are measured in the linear range.
- For viscous materials flow is linear even under high stress and high strain.
- For polymer networks the binder response is not linear for high stress and high strain.

# High Temperature Binder Criteria

## ■ Study

- Evaluate several binders in the same mix
- Evaluate binders in rut testers
- Hamburg wheel tracker
- Asphalt Pavement Analyzer

# Rutting in Asphalt Layer

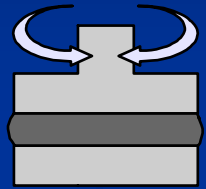
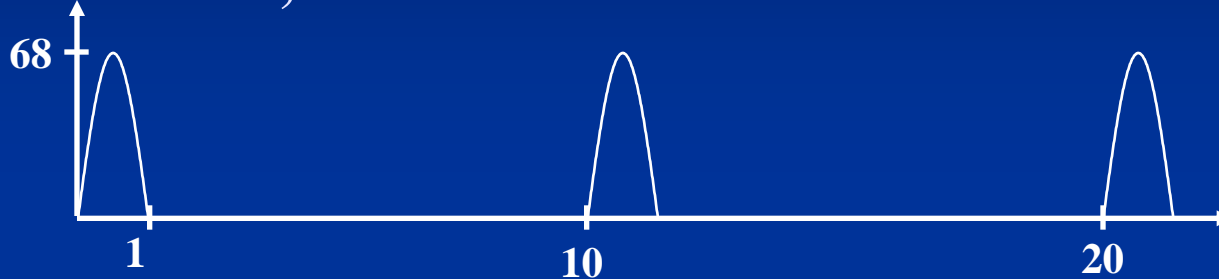


Movement and rotation of aggregate creates very high strain in the binder.

# NCHRP 9-10 Rutting Test

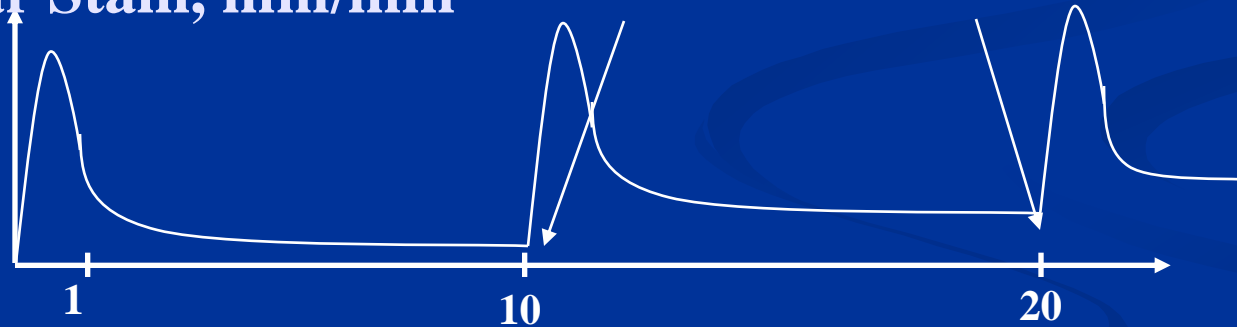
## Repeated Creep Recovery Test

Shear Stress,



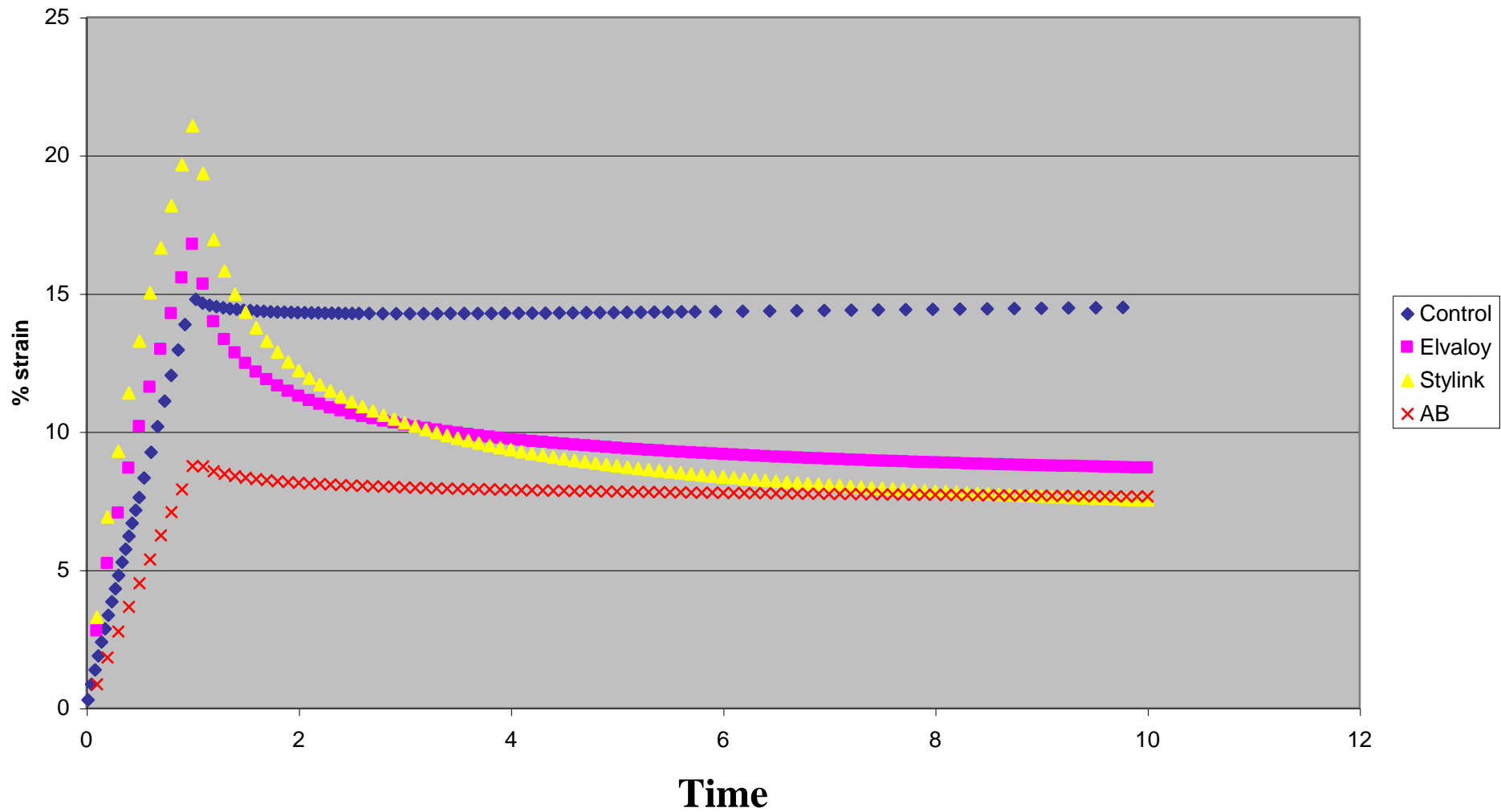
Shear Strain, mm/mm

**Accumulated Strain**

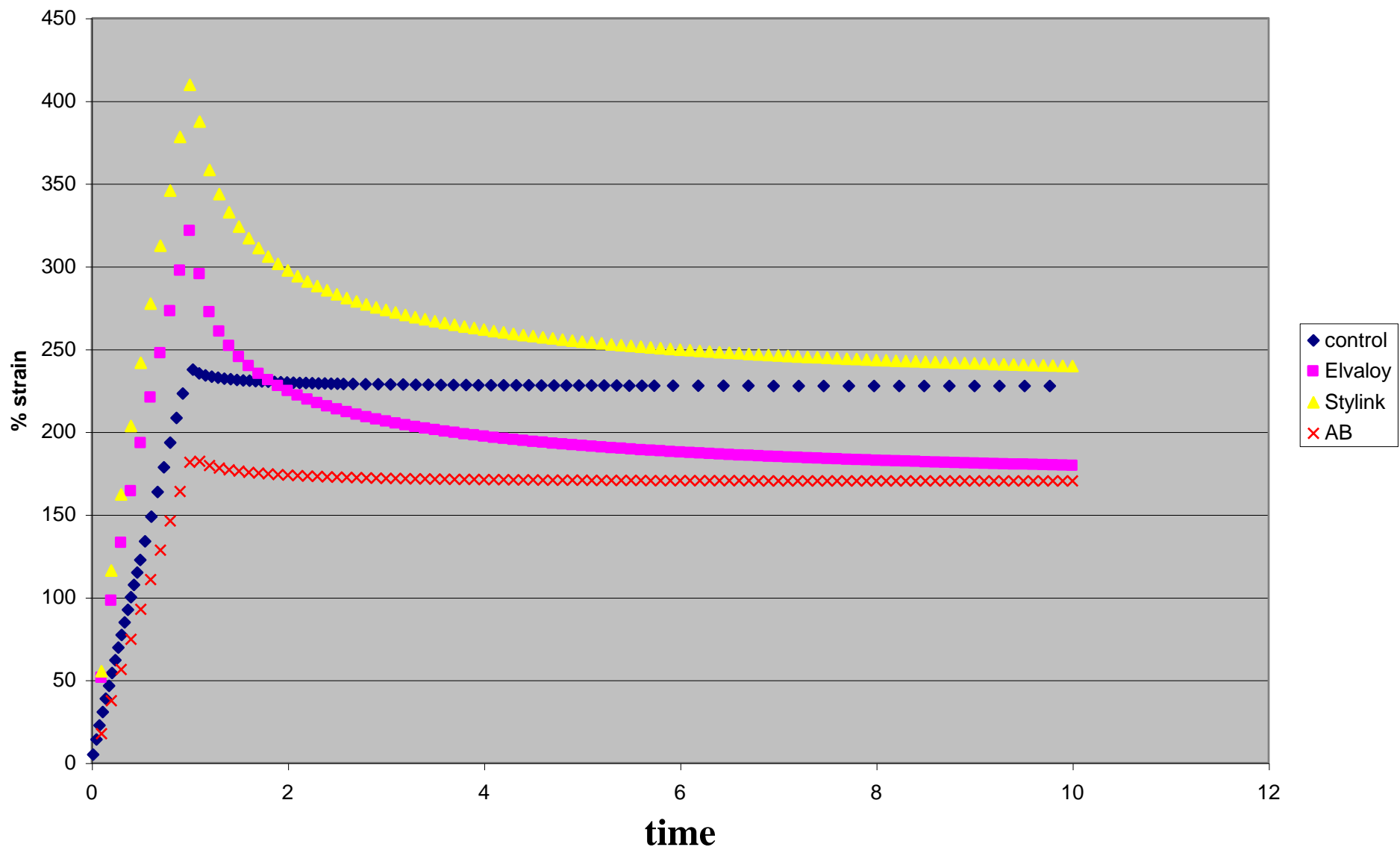


The original 9-10 work included only one stress level. Future work to look at multiple levels.

# Creep 1st cycle 70C 50 Pa



## Creep 1st cycle 70C 1000 Pa



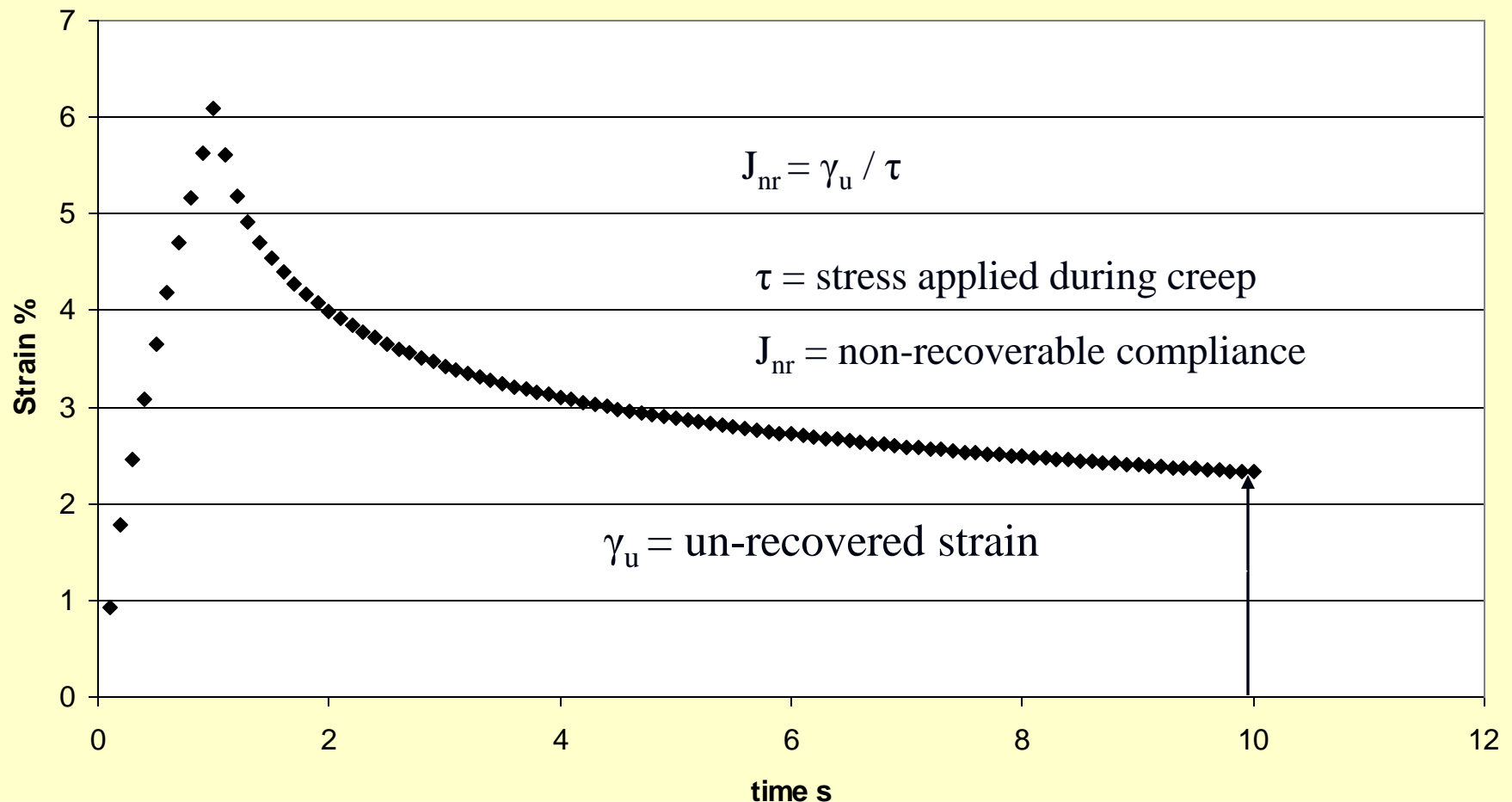
# High Temperature Binder Criteria

- APA and Hamburg are failure tests.
- Binder properties measured in the linear range can not correlate with non linear mix tests.
- Polymer chains will slip under high stress and allow high strain
- Pavement response must be determined to relate binder to mix

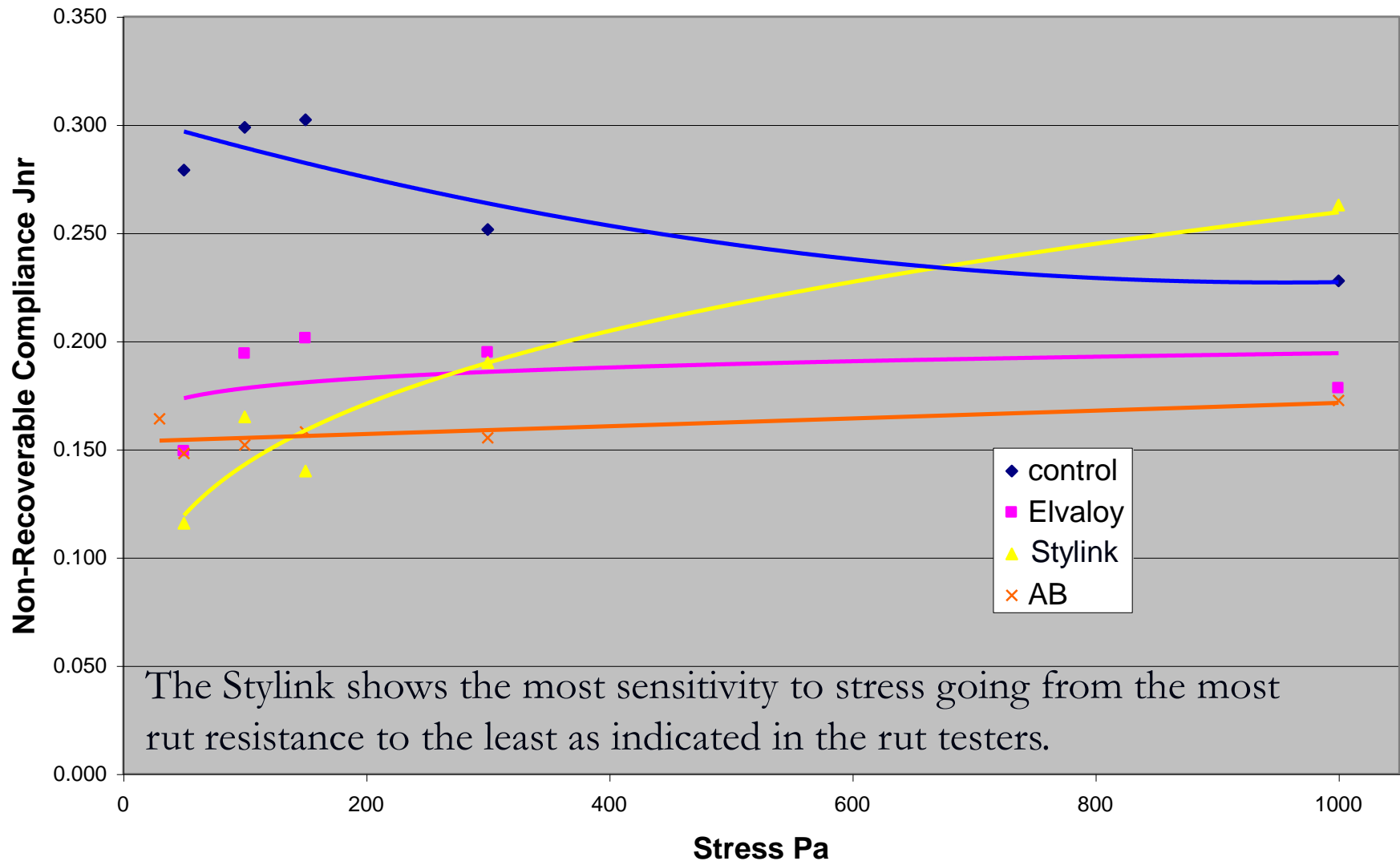
# High Temperature Binder Criteria

- New criteria non-recoverable compliance is based on binder creep testing at several stress levels.
- Determine the average non-recovered strain at a specific stress level and then divide the average non-recovered strain by the initial stress = non-recoverable compliance  $J_{nr}$ .

# What is Non-recoverable compliance



# Jnr of the binder from Rut Tester Study



# High Temperature Binder Test

- New experimental test criteria:
  - Perform multiple stress levels on the same sample at reduced number of cycles.
  - Stress levels: .025, .05, .1, .2, .4, .8, 1.6, 3.2, 6.4, 12.8, 25.6 kPa.
  - Run 10 cycles at each stress level no rest periods
  - Total cycles per test 110.

# High Temperature Binder Criteria

- New test criteria:
  - Does the strain of the multi-step compare to the individual test?
  - Does the reduced number of cycles per stress level compare to the individual test at greater number of cycles?

# Polymer Binder response to stress

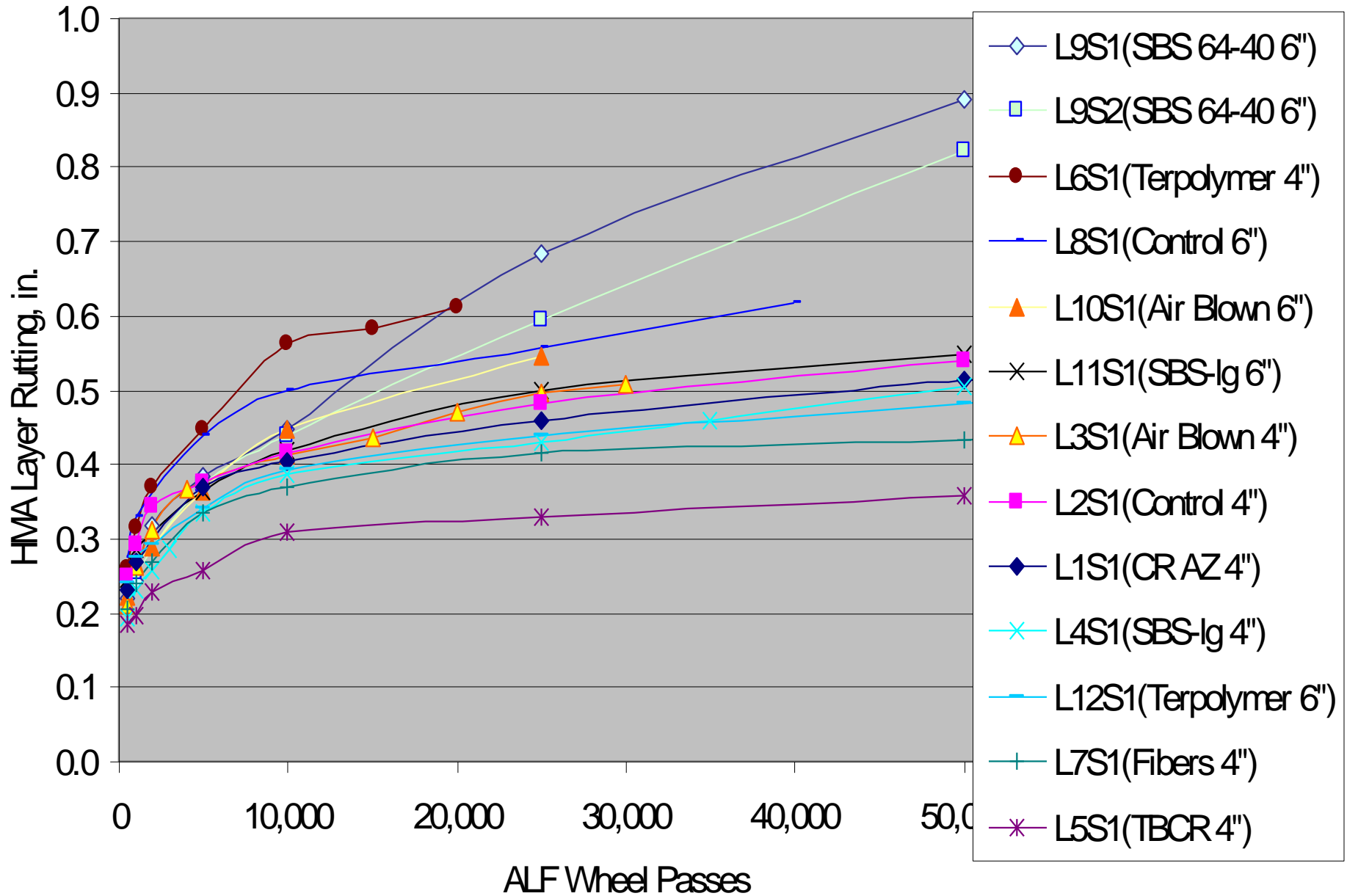
- Polymer binders are basically a two phase system made up of polymer dispersion in a viscoelastic solution typically a neat asphalt binder.
- How this combination responds to loading is greatly affected by the base binder, the entanglement of the polymer chains and any cross linking in the polymer network.

# 7 Asphalt Binders

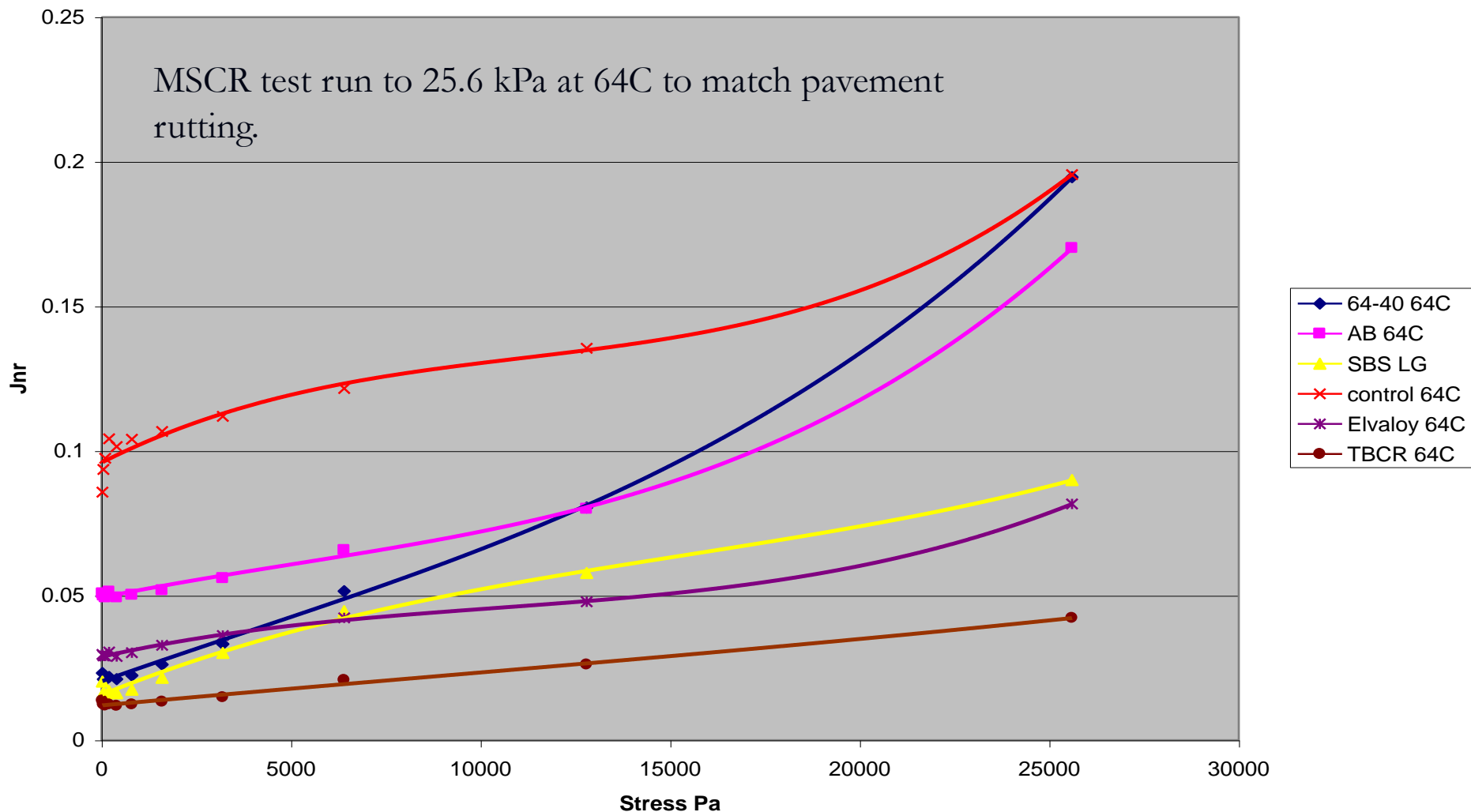


AZ CRM ---- 70-22	PG 70-22 Control	Air Blown	SBS	TX TBCR	TP	PG 70-22 + Fibers	PG 70-2264-40	SBS 64-40	Air Blown	SBS	TP
1	2	3	4	5	6	7	8	9	10	11	12

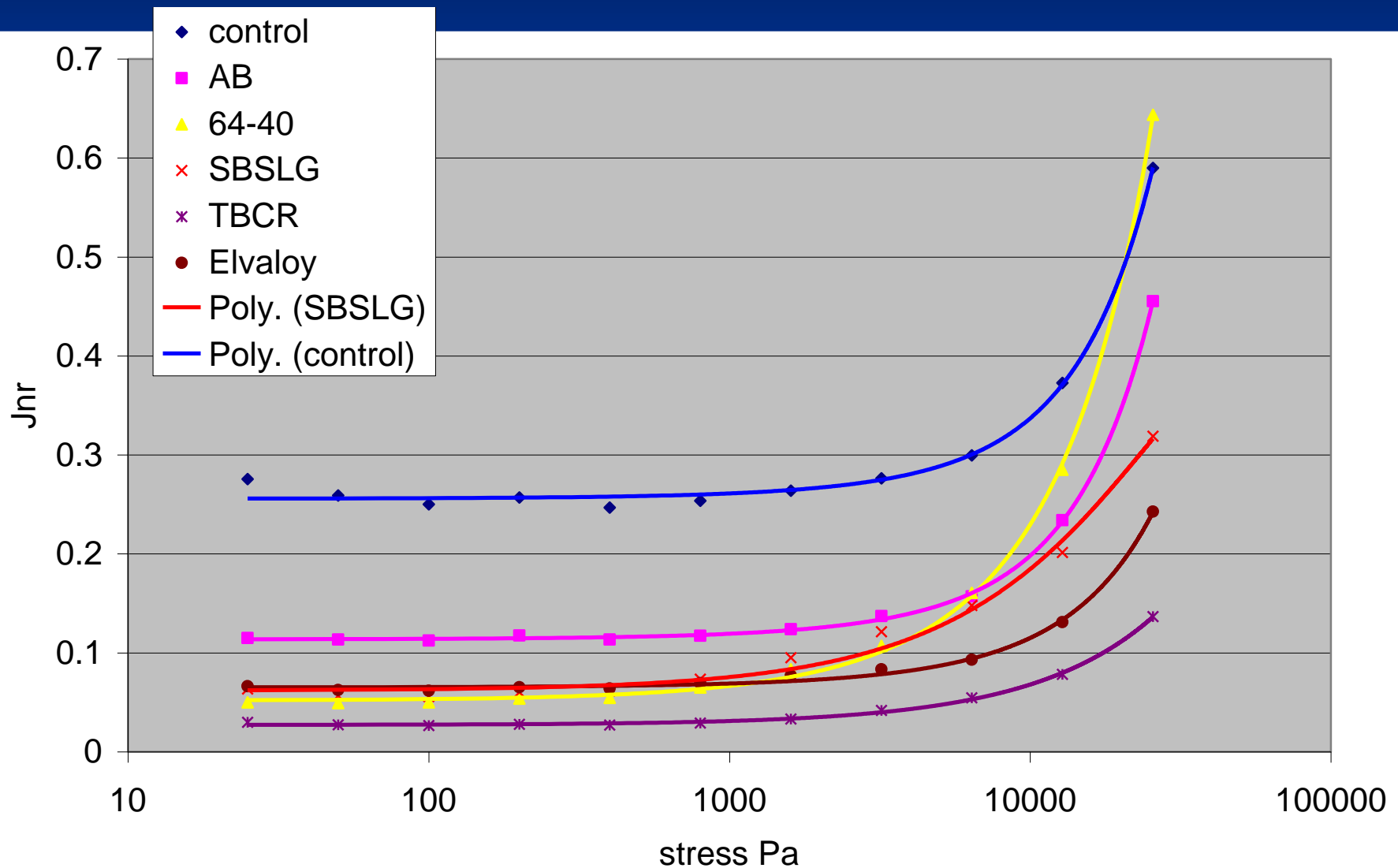
## HMA Layer Rutting for All Lanes



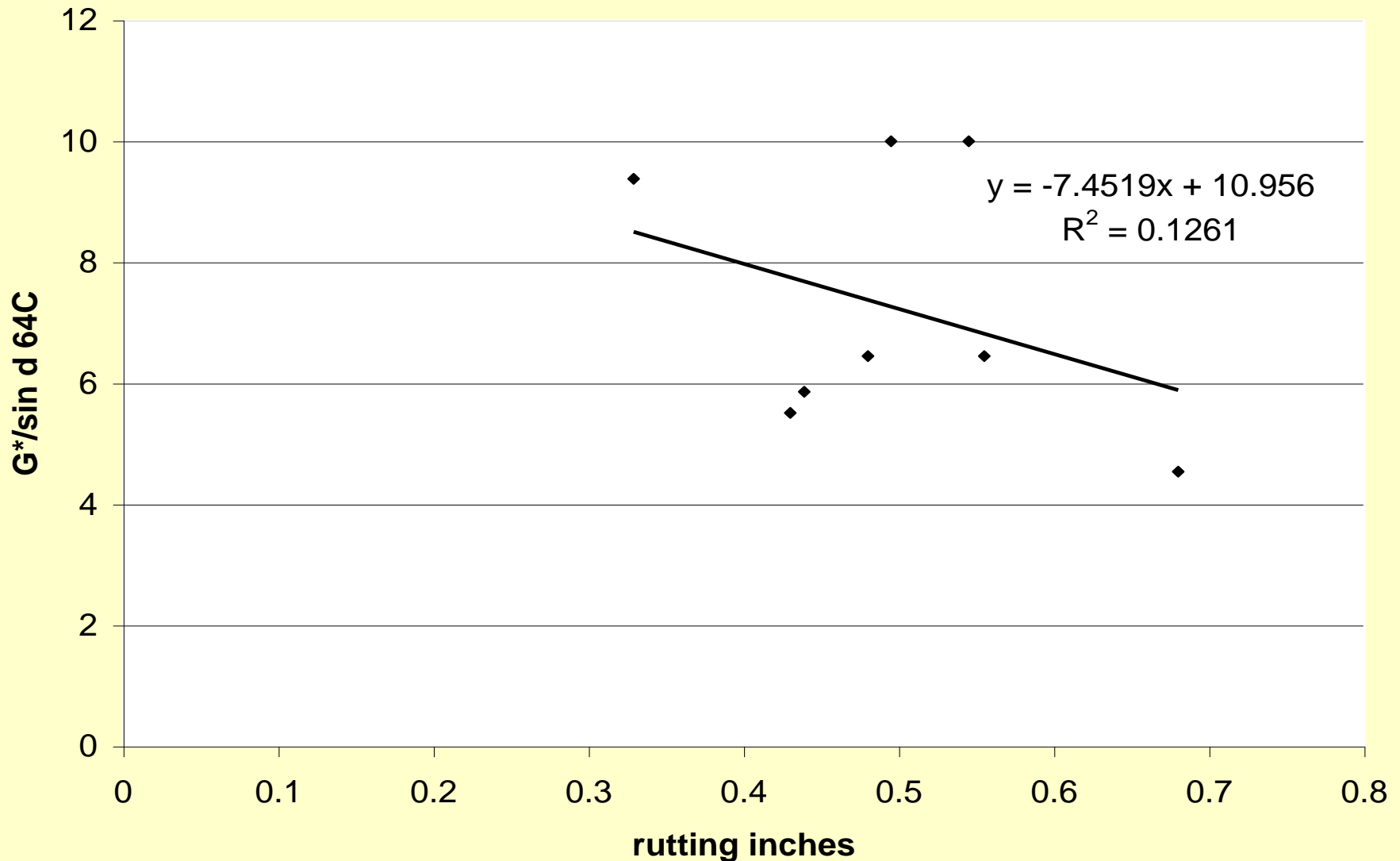
# Non-Recoverable compliance on the polymer binders tested in the ALF sections



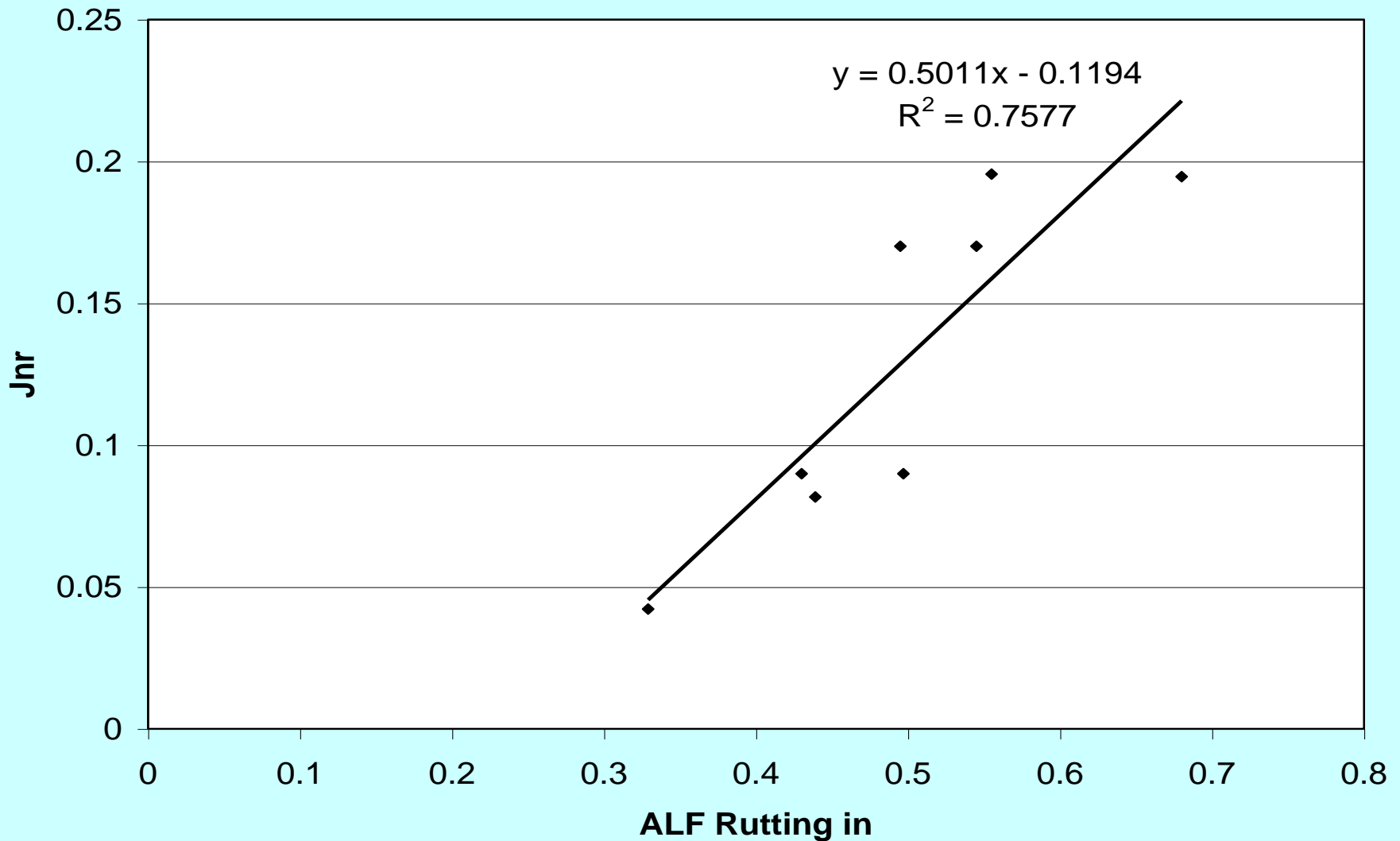
# ALF binder @ 70C



# Relationship between $G^*/\sin\delta$ and ALF rutting



# Relationship between Jnr and ALF rutting



# High Temperature Binder Criteria

## ■ Conclusion

- Linear binder tests will not correlate with high temperature mix failure test unless the binder is a viscous fluid at those temps.
- To accurately address mix failure non-linear binder properties have to be evaluated.
- Creep & Recovery testing of the binder at different stress levels is needed to describe binder properties in the non-linear range.

# High Temperature Binder Criteria

## ■ Conclusion

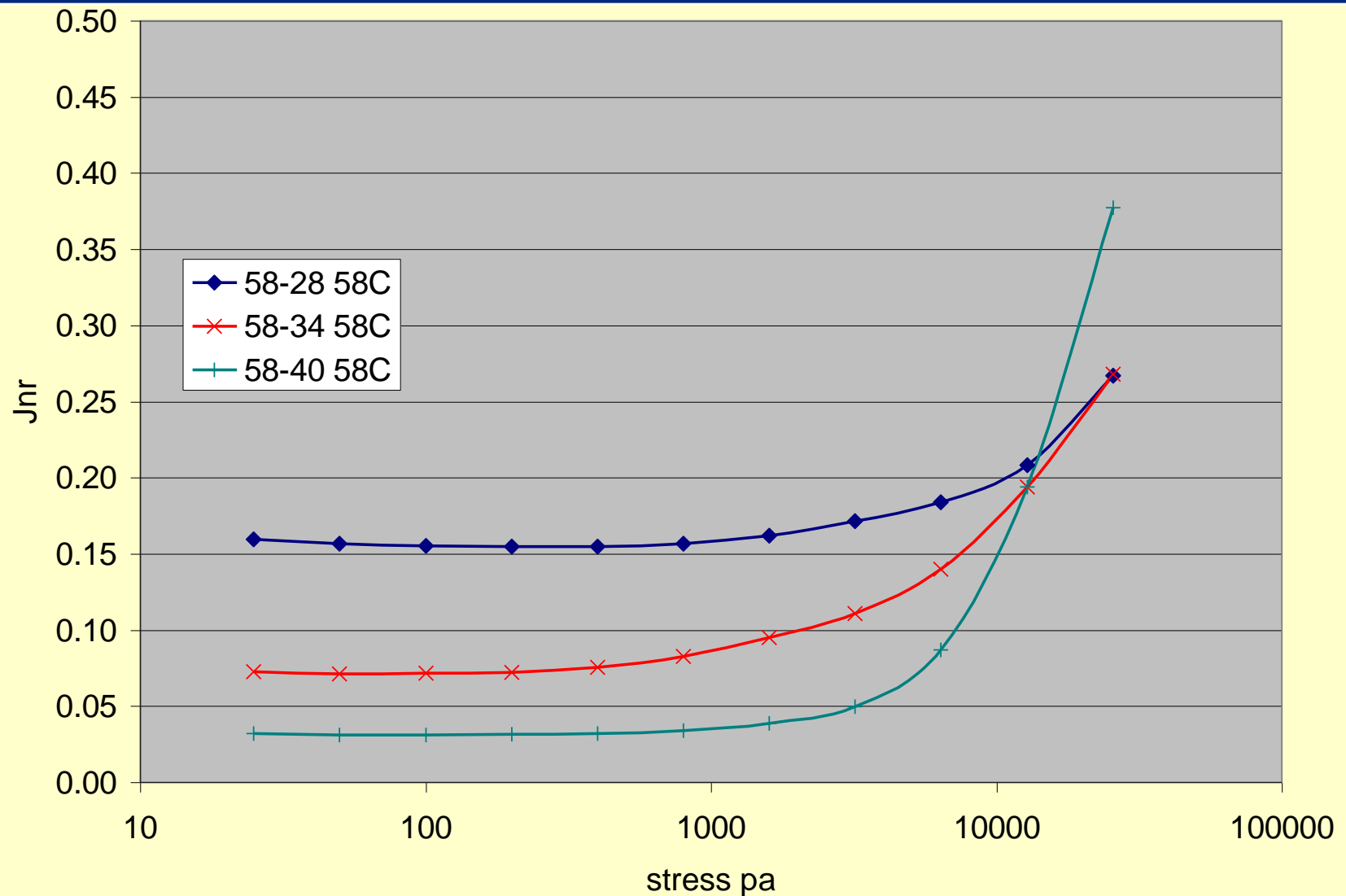
- Non-recoverable compliance of the binder describes the stress dependency of the binder.
- Creep and recovery run at multiple stress levels on one sample can be run to describe the stress dependency of the binder.
- Creep and recovery non-recoverable compliance can be correlated to mix testing done at different stress conditions.

# High Temperature Binder Criteria

## ■ Recommendation

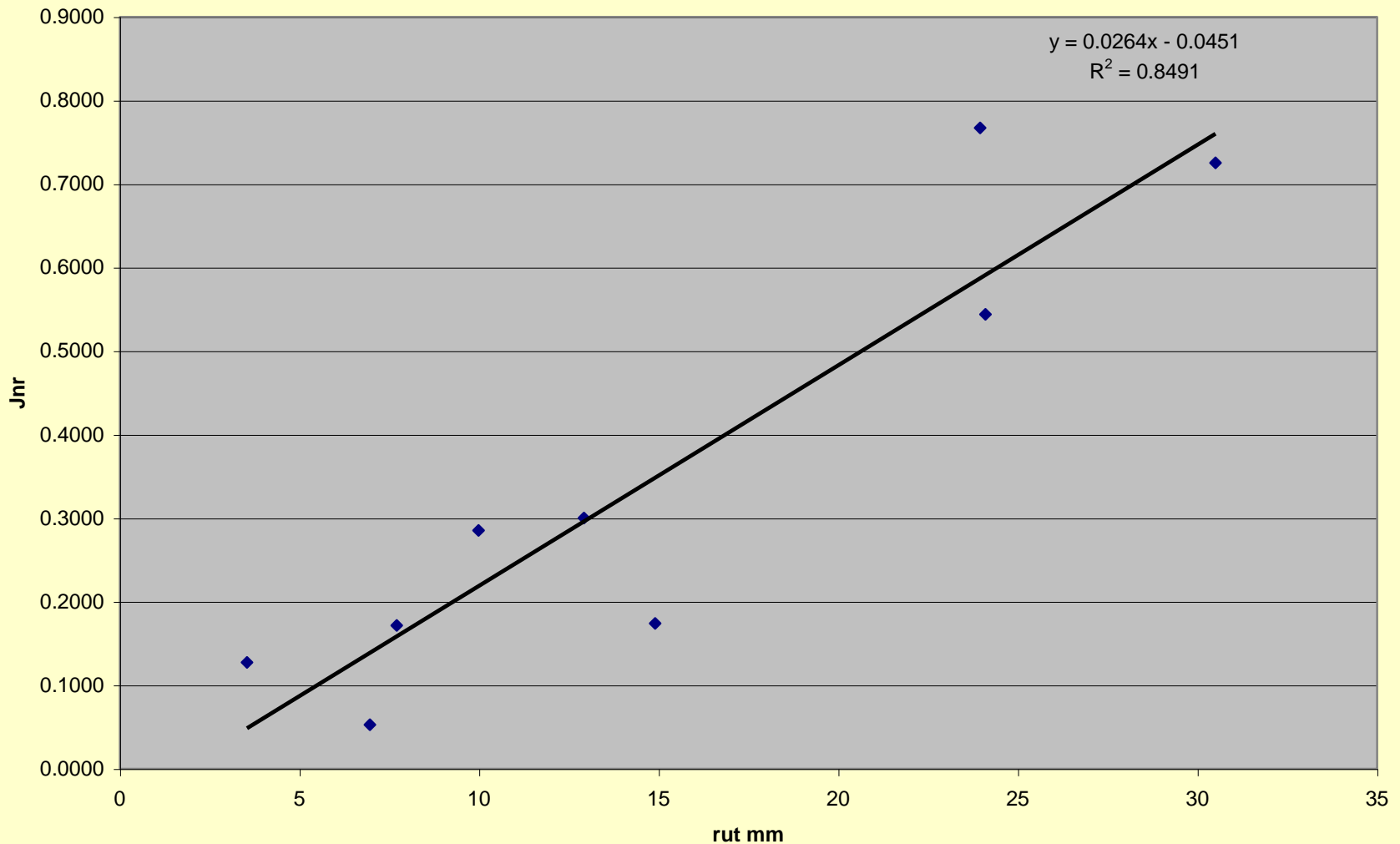
- Test more binders with various modification systems to finalize test procedure.
- Evaluate binder results against mix testing to determine the relationship of rate of change of compliance to mix performance.

# MinnRoad Binders

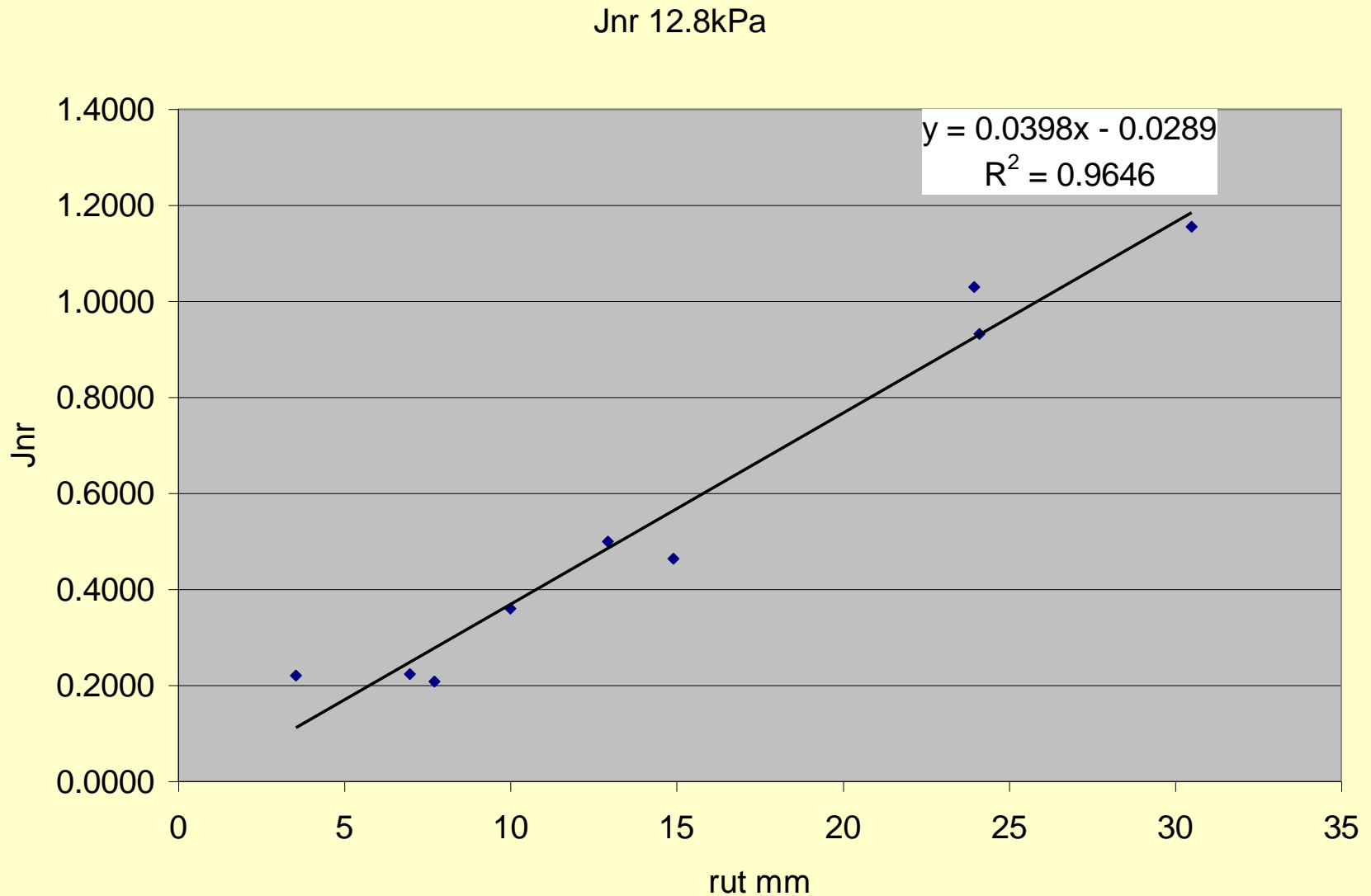


# Hamburg Rut testing MINN Road mixes

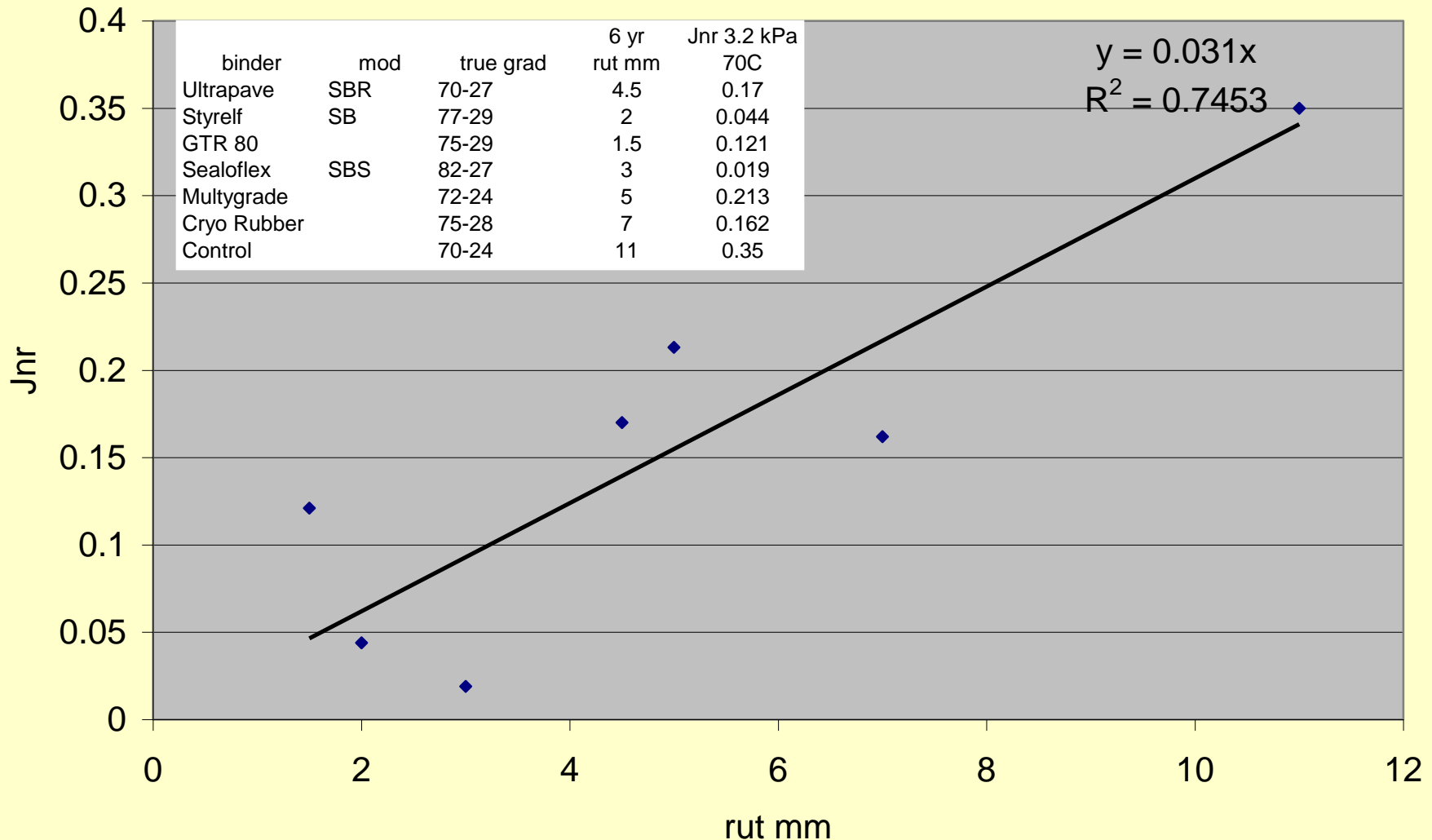
Jnr3200Pa



# Hamburg Rut testing MINN Road mixes



# Miss I55 6yr rut Jnr 3.2 kPa



# Affect of Jnr on Rutting

- Reducing Jnr by half typically reduced rutting by half.
- This affect is seen on ALF sections, Hamburg Rut Testing
- But most importantly this is seen on the Mississippi I 55 sections.

# Neat Binder Response

- Neat binders linear over a wide range of stresses and strains.
- Most neat binders remain linear up to 3.2 kPa stress.

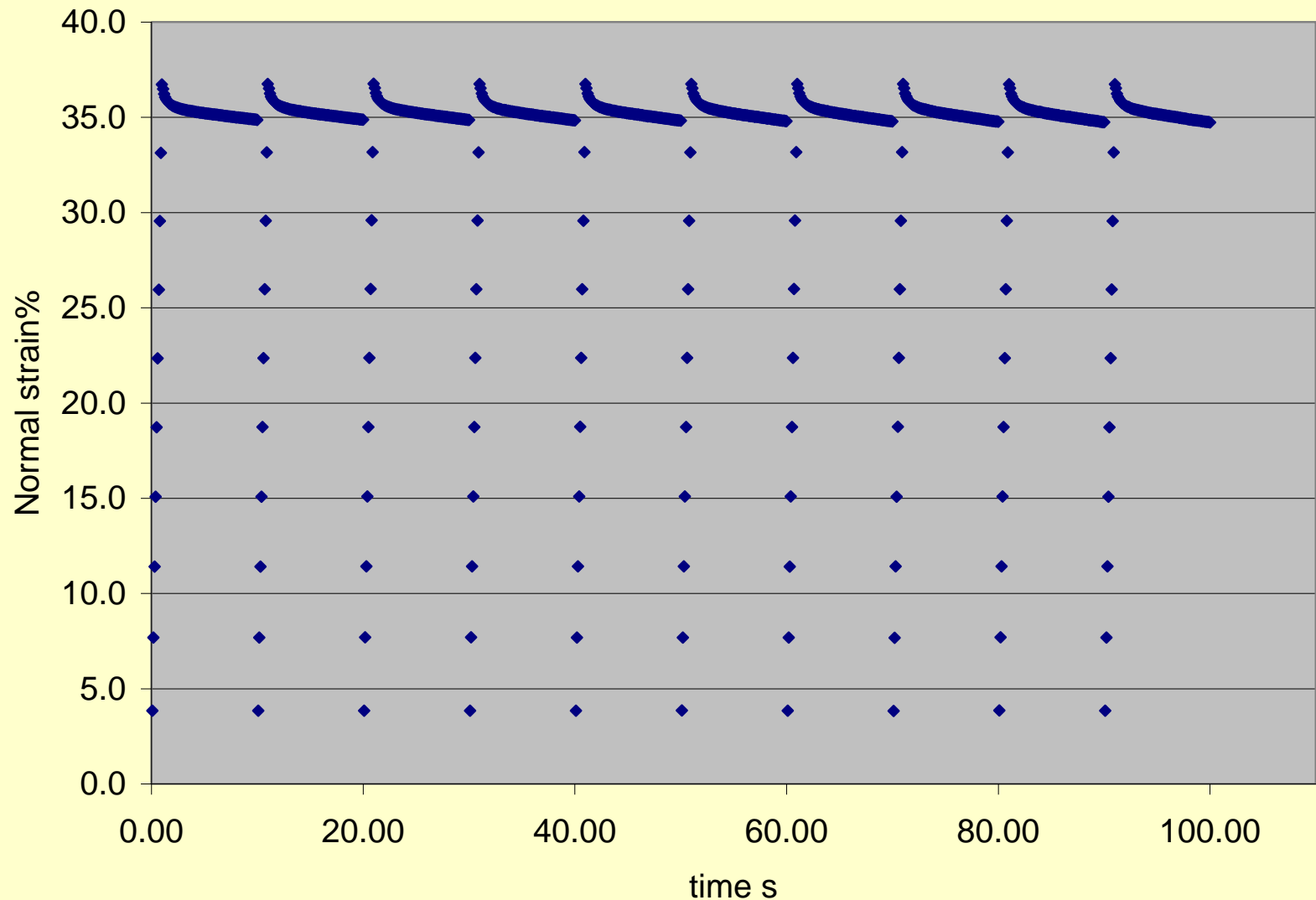
# Determination of a Specification criteria.

- The existing binder specification works very well for neat binders.
- The grading for neat binders should not change.
- Establish new Jnr criteria based on response of neat binders at their continuous grade temp.
- Evaluate the binders near the end of their linear range.

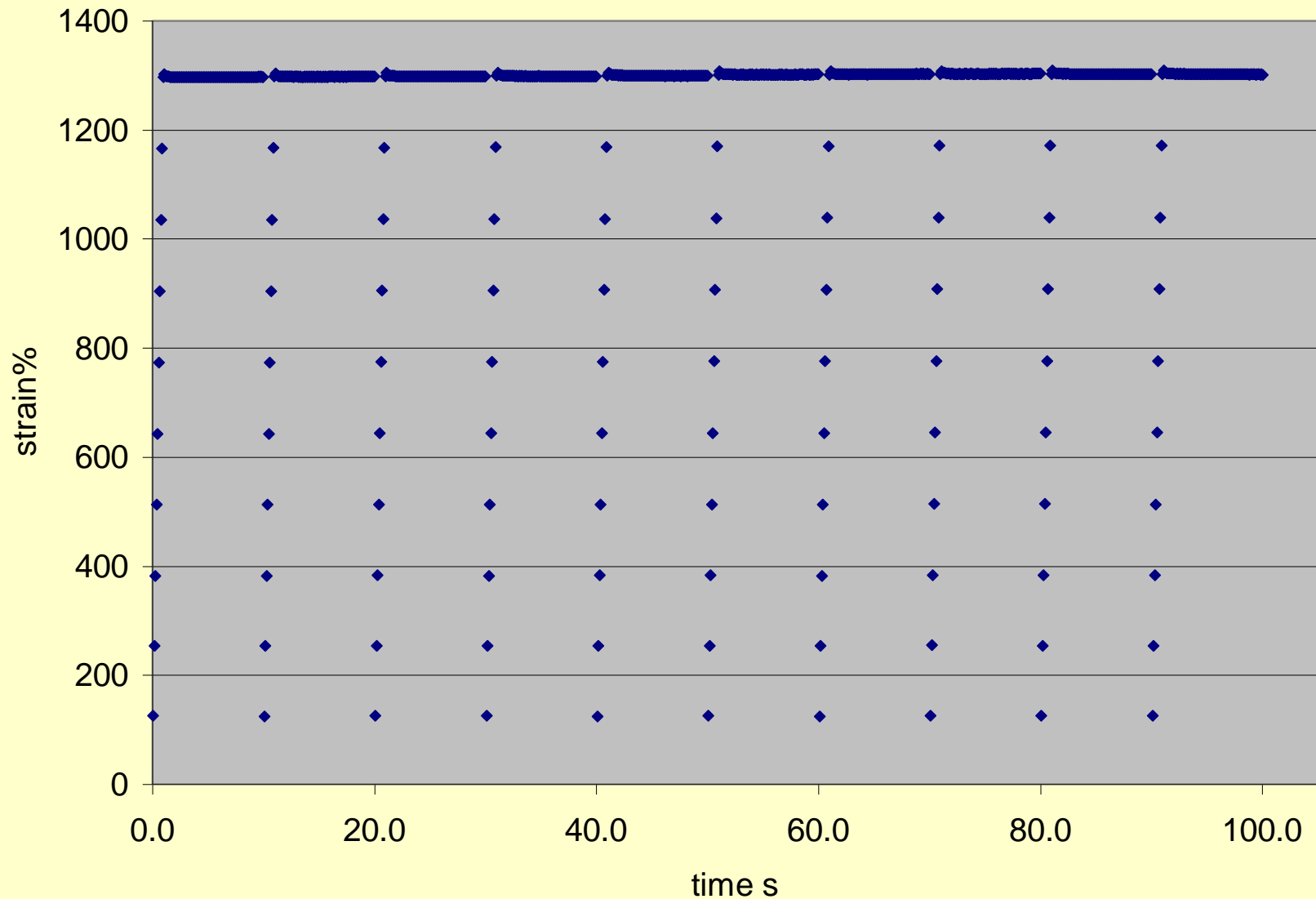
# Evaluation of Straight run binders

Sample ID	Name	Grade	true grade	Temp	Jnr 3200Pa
ALF 6727	Control	70-22	72.7-74.2	72.7	0.439122
BBRS3	straight	64-22	66.1-27.3	66.1	0.418449
MN county rd 112	neat Valero	58-28	60.8-33.4	60.8	0.368445
MN county rd 112	neat Citgo	58-28	59.5-29.8	59.5	0.529647
MN county rd 112	AshlandM	58-28	60.7-31.4	60.7	0.430165
Minn Road	straight	58-28	61.8-30.8	61.8	0.302951
Miss I-55	CSL	67-22	68.3-25.1	68.3	0.266912
Shandong	straight	64-22	64.4-23.5	64.4	0.444057
BBRS3	straight	70-22	71.4-24.8	71.4	0.480855
BBRS3	straight	58-28	61.3-30	61.3	0.400345
MD project	straight	64-28	64.8-29.6	64.8	0.459335
average					0.412753

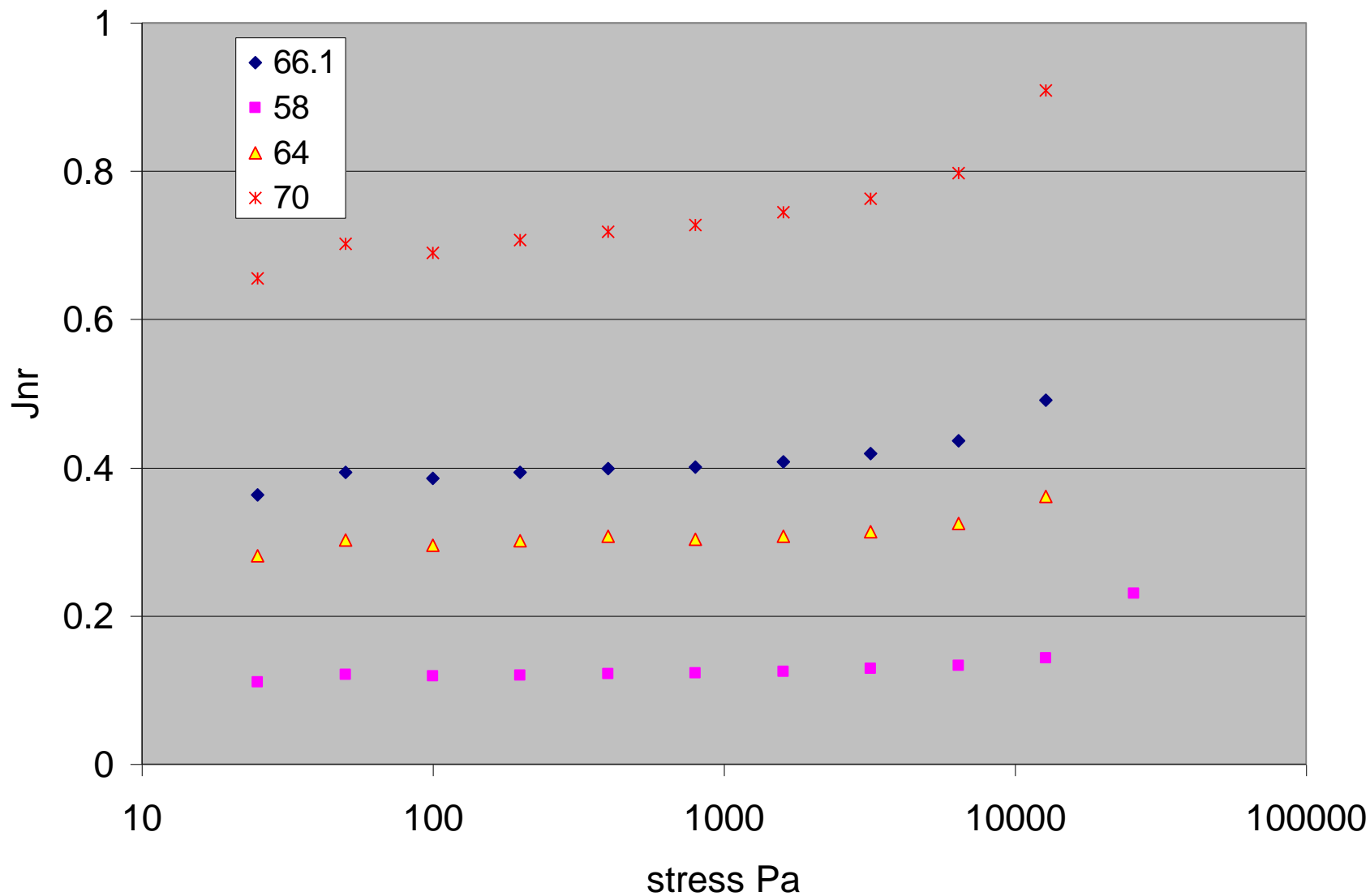
# Neat PG 70-22 @ 70C 0.1 kPa



# Neat PG 70-22 @ 70C 3.2 kPa



# BBRS3 PG 64-22



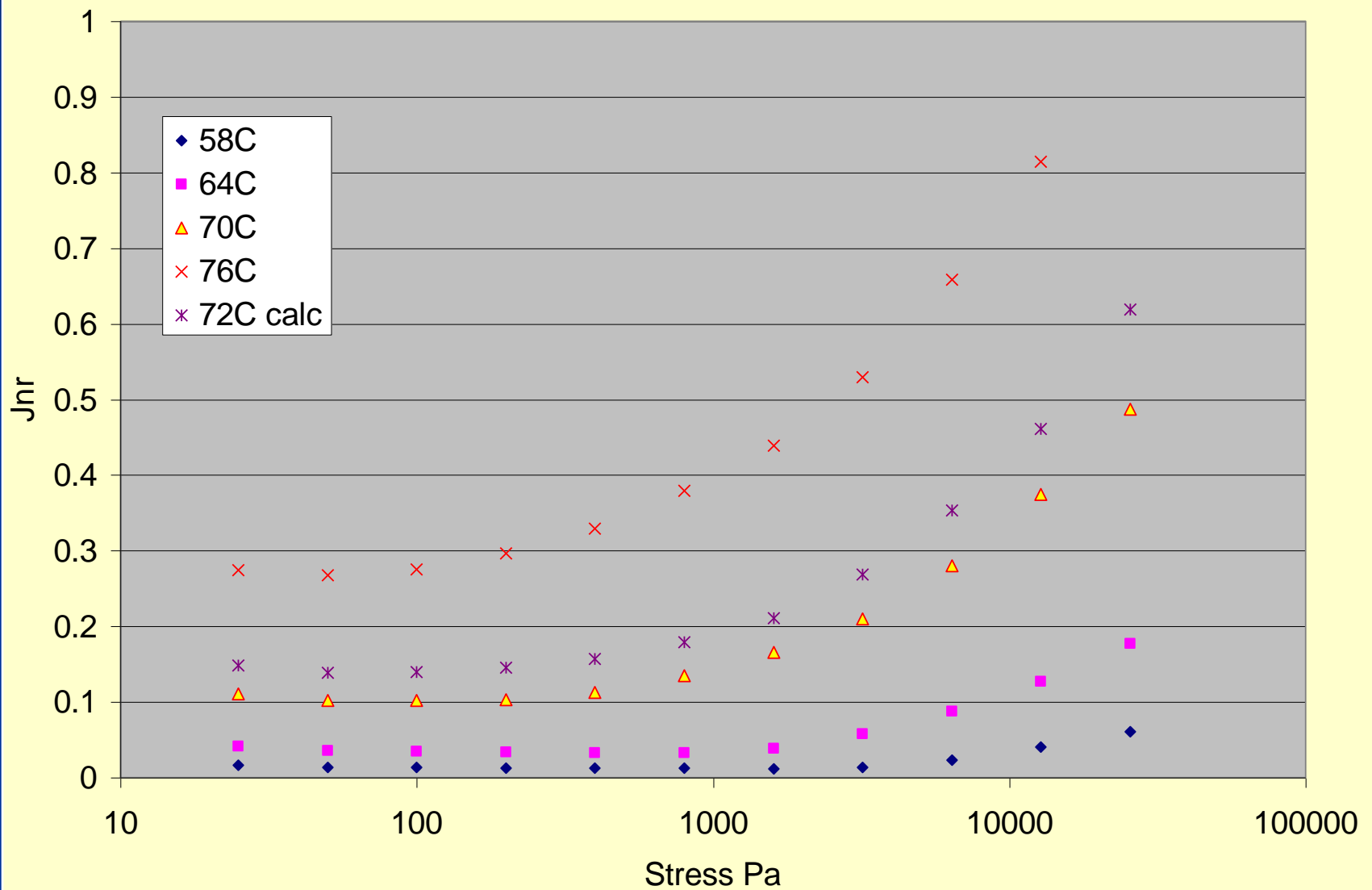
# Determination of a Specification criteria.

- The average  $J_{nr}$  of many neat binders at their continuous grade temperature is 0.4
- Use  $J_{nr}$  of 0.4 at 3.2 kPa as the specification criteria.

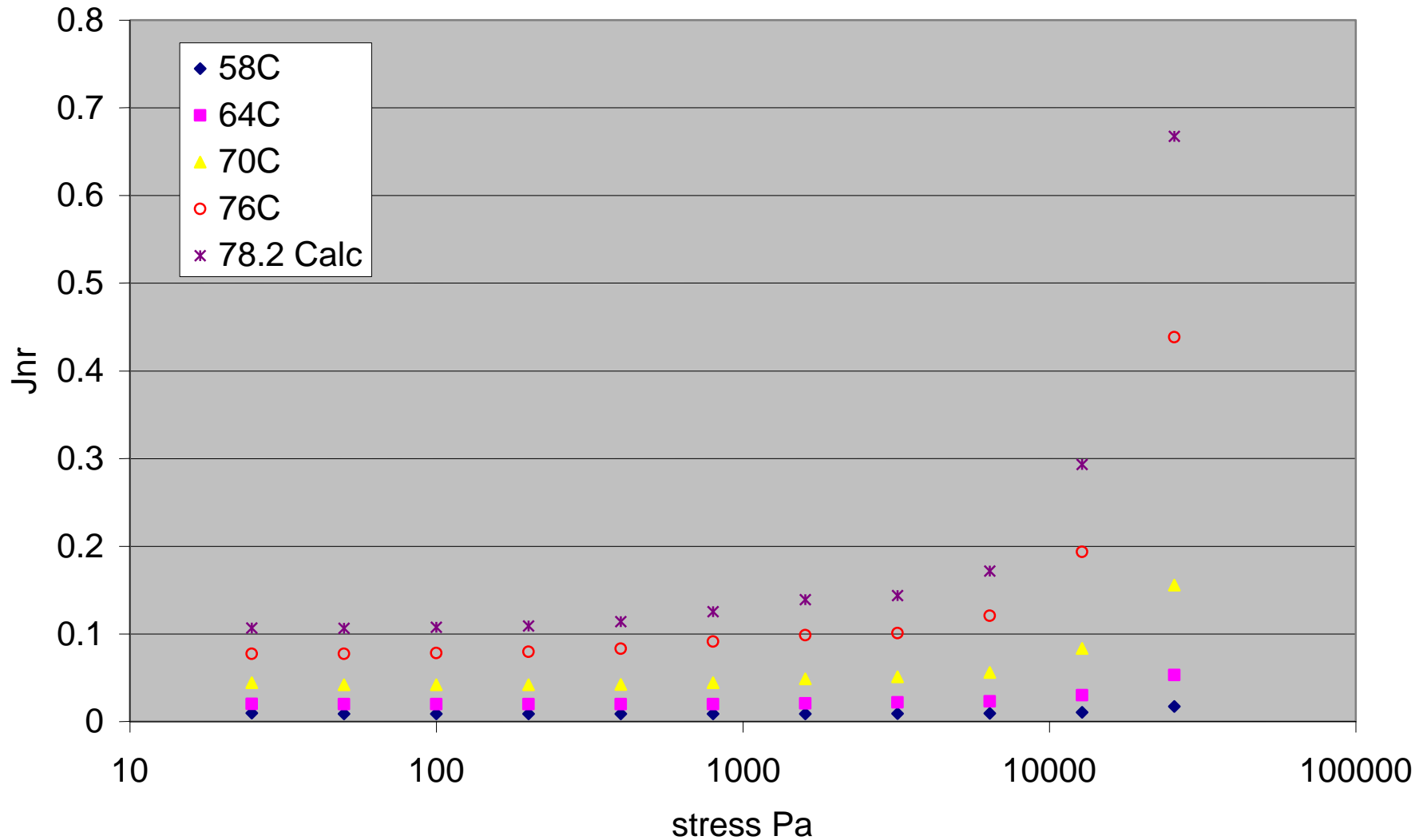
# Grade Bumping and how it would work

- The existing system uses temperature to adjust for increased traffic or slower traffic speeds.
- Should the new criteria use the same system or is there a better way?
- The first step is to see how the existing polymer systems have worked

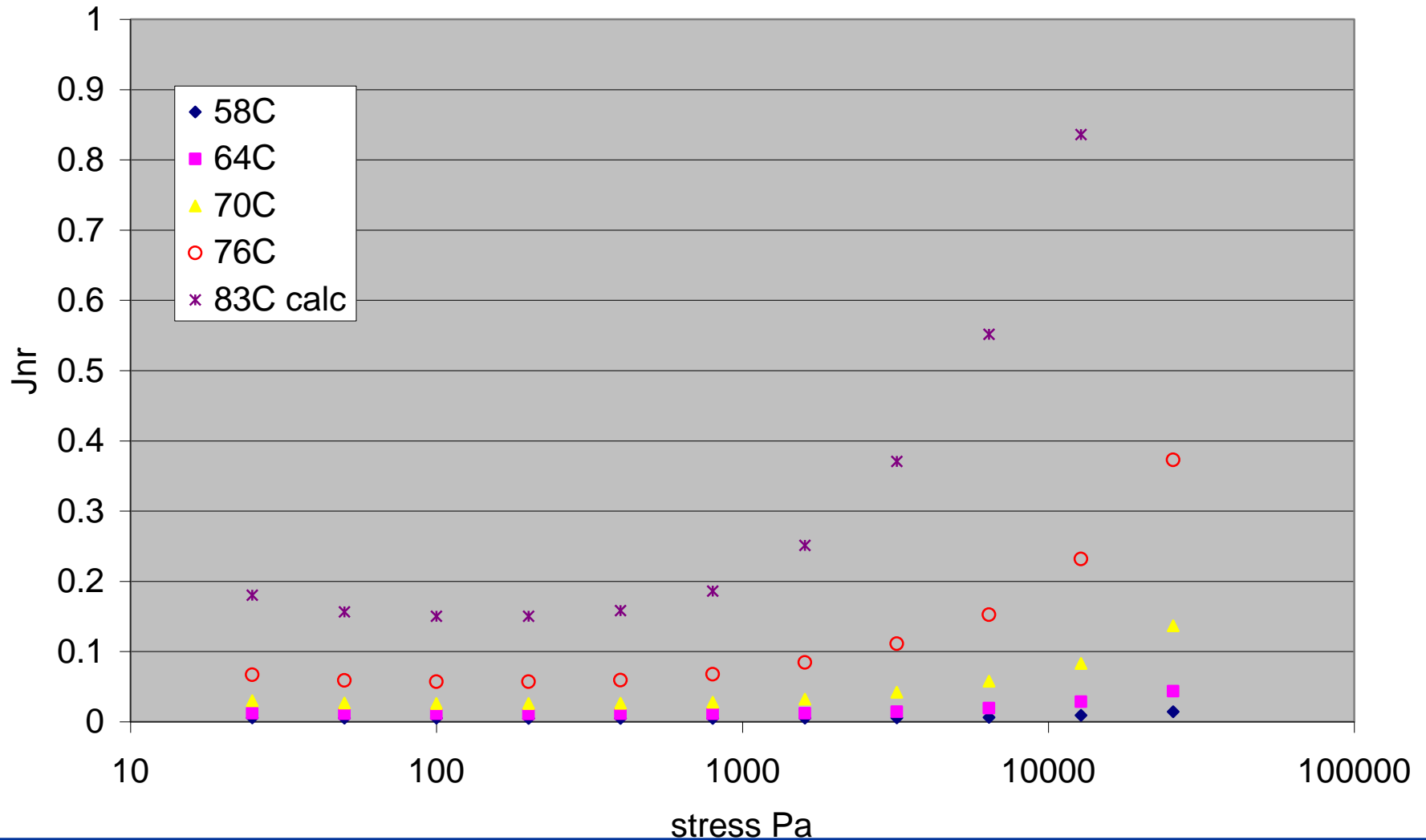
# SBS PG 70-28



# Elvaloy PG 76-28



# Ergon PG 82-22



# Affect of Temp and Stress on Jnr

- In neat binders a grade bump by temp will more than double the Jnr value.
- Some neat binders will maintain their compliance value well beyond the 3.2 kPa stress.
- Grade bumping by increases in PG grade temp have forced suppliers to use very soft base binders and high degree of polymer modification to meet wide temperature ranges.
- This has made some polymers very stress sensitive.

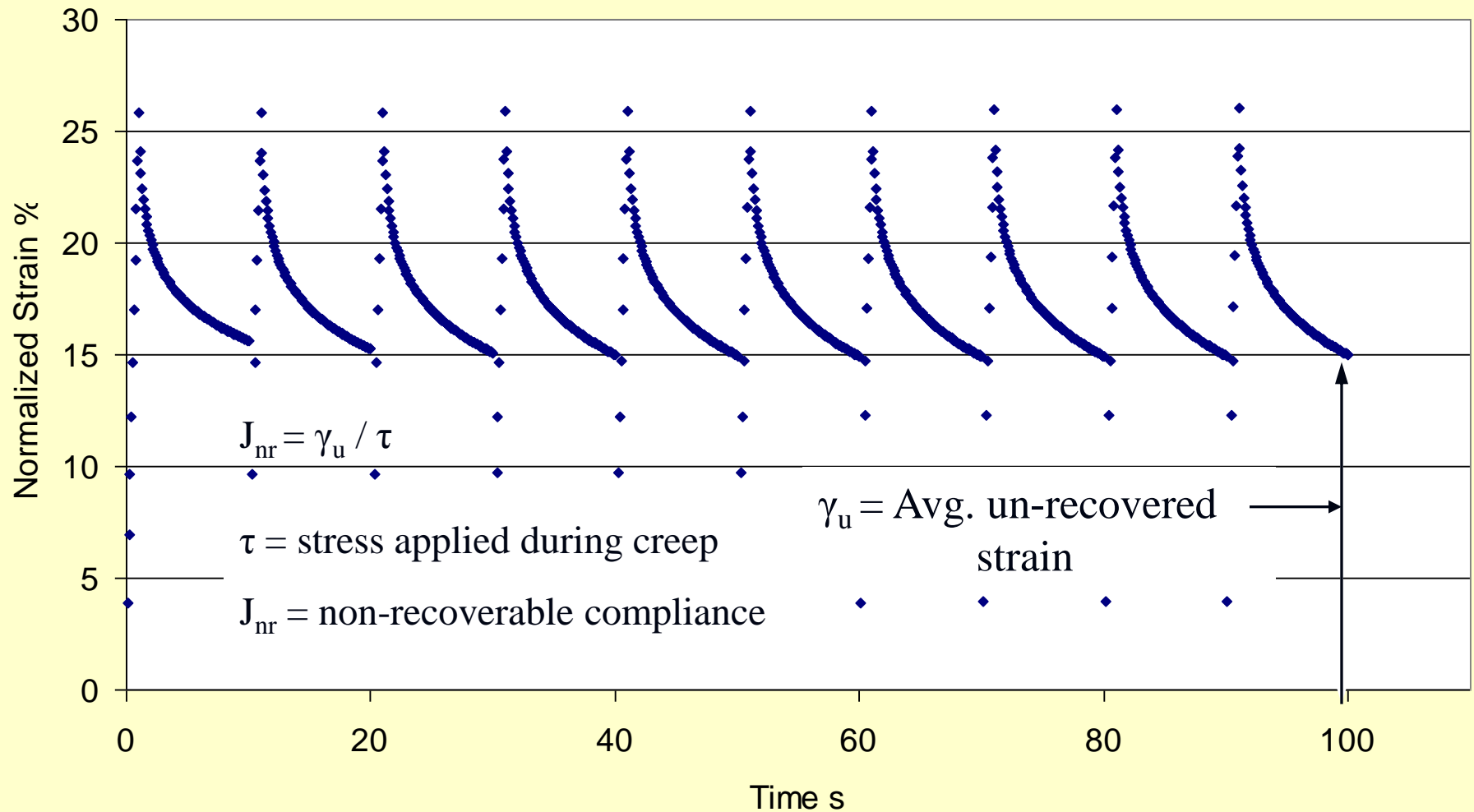
# Grade bumping recommendation

- All testing should be done at the environmental grade temp.
- The standard grade should be based on the Jnr value of existing neat binders.
- For high traffic the Jnr value should be reduced by half at the grade temp.
- For standing traffic the Jnr value should be reduced by half again.

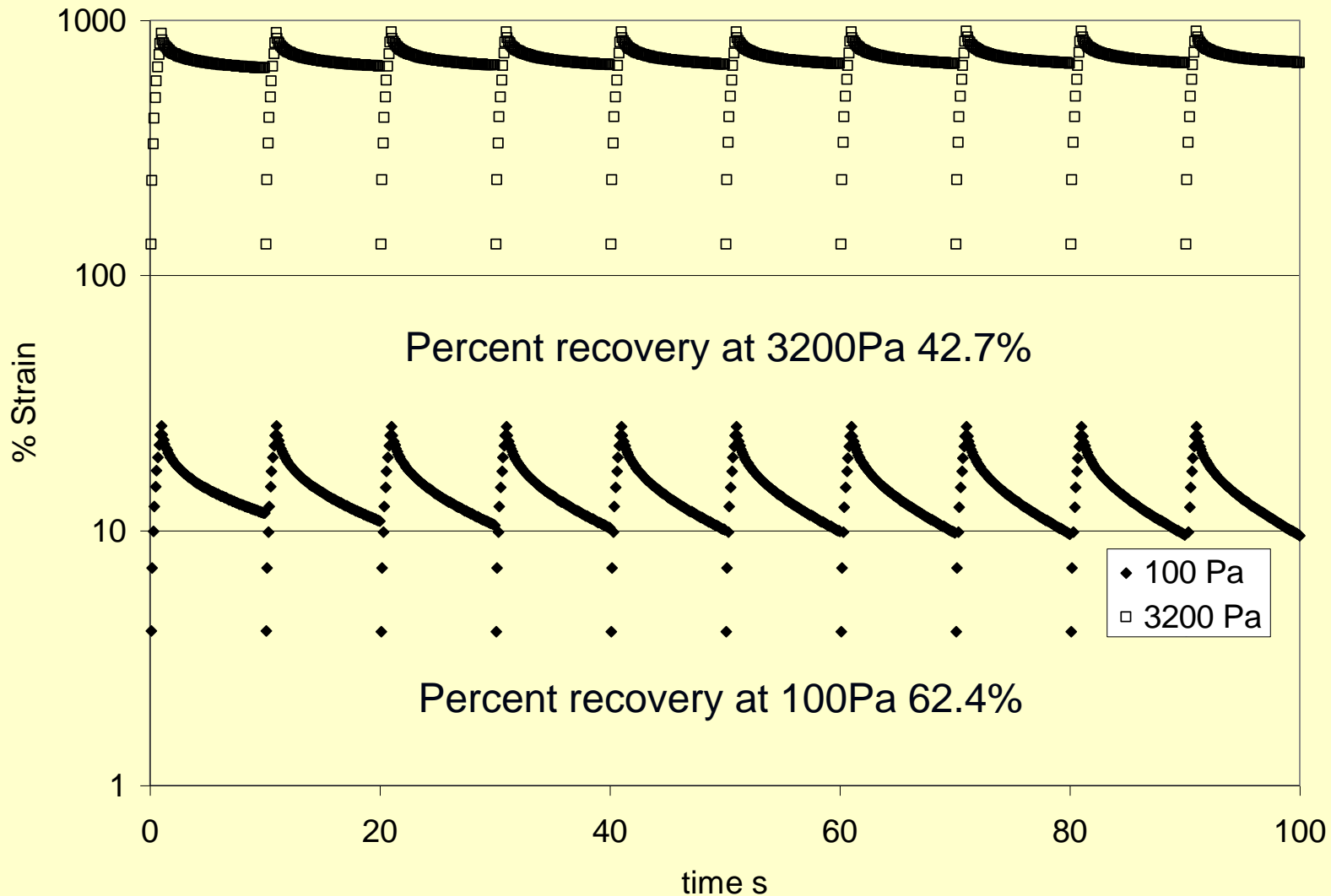
# New High Temperature Binder spec

- The new specification should be based on the non-recoverable compliance on the binder.
- All testing should be done at the pavement environmental grade temp
- The test should be run at two stress levels 0.1 and 3.2 kPa ten cycles at each level. A comparison would be made to check how stress sensitive the binder is.
- Grade bumping should be done by halving the  $J_{nr}$  value.

# Determination of $J_{nr}$



# New High Temp Spec Verifies Polymer Use



Thank You